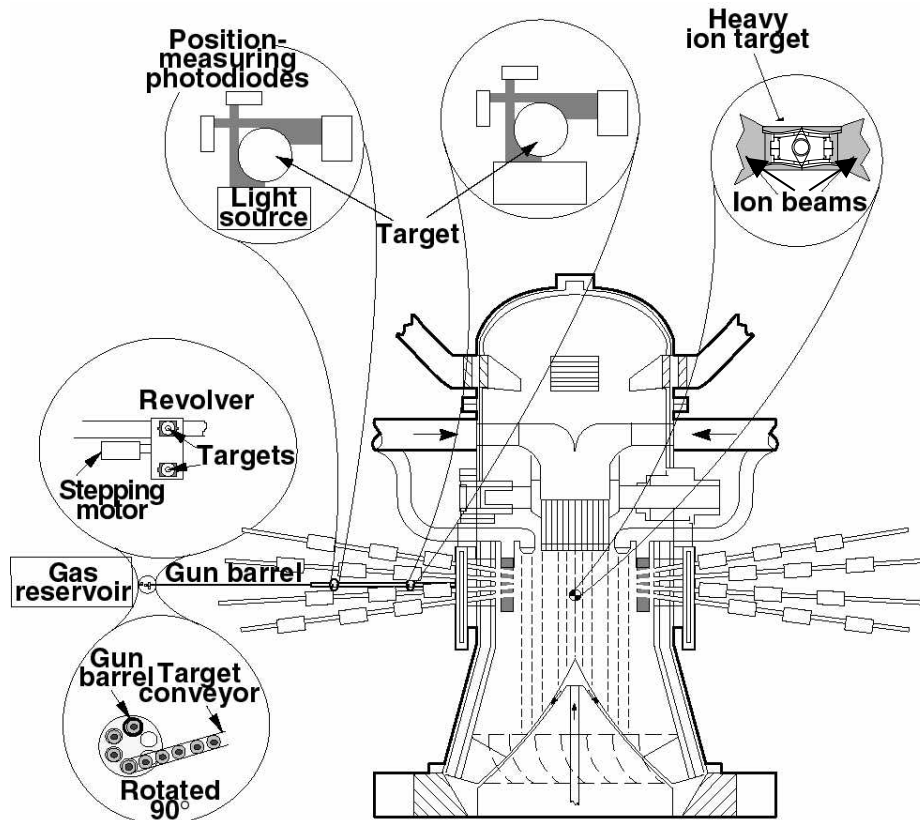


# Indirect Drive Target Injection



**Summary:**  
Target Structure for Acceleration  
Target Heating  
Fluorine Diffusion  
Tracking/Positioning

Ronald Petzoldt  
ARIES IFE meeting, UCSD, La Jolla, CA

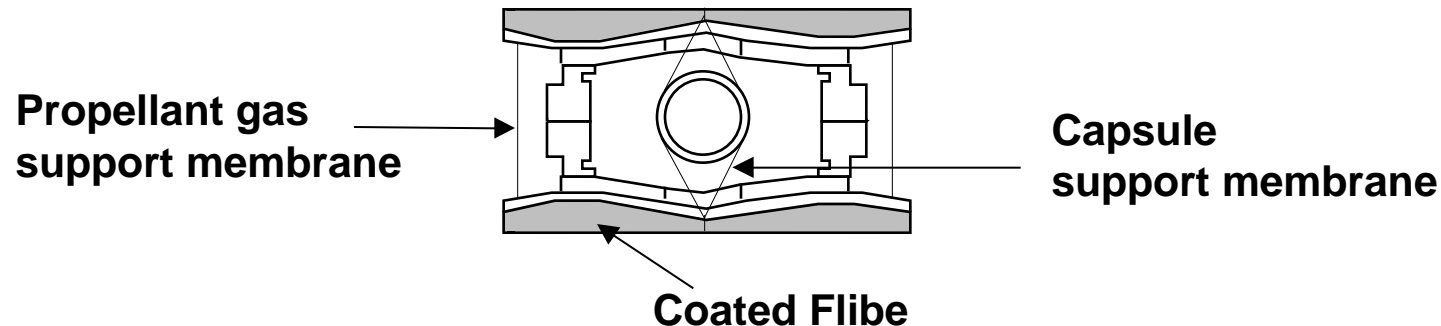
8 June 2001



# The target's structure must support acceleration

Target acceleration  $\sim 2500 \text{ m/s}^2$

Barrel length =  $v^2/2a \sim (100 \text{ m/s})^2/[2(2,500 \text{ m/s}^2)] = 2 \text{ m}$



Flibe mechanical properties are unknown but may be similar to other salts

Low density foam properties are unknown

DT strength will be measured at LANL

(extrapolated DD properties indicate  $10,000 \text{ m/s}^2$  acceptable)

Gas support membrane thickness for  $2,500 \text{ m/s}^2$  is  $\sim 4$  microns.

(4 microns absorbs about 1% of beam energy)

Capsule support membrane thickness  $\sim 0.2$  micron\* for  $2,500 \text{ m/s}^2$

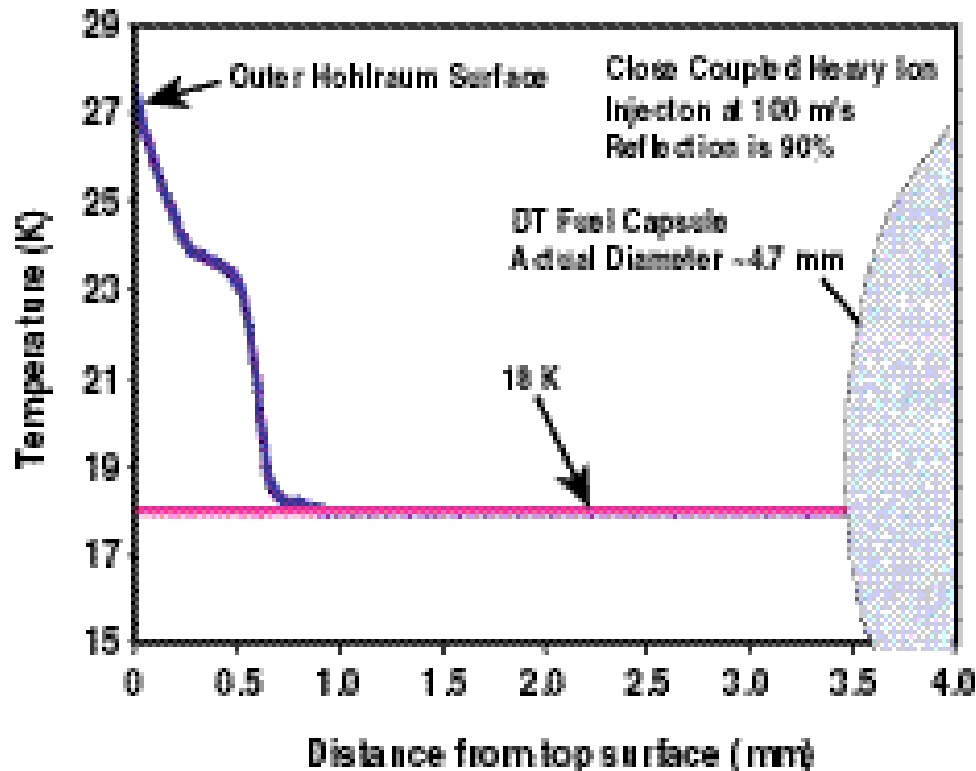
Capsule displacement  $\sim 100$  microns can be reduced by pre-stressing membranes

\*R. W. Petzoldt & R. W. Moir,

Membrane Support of Accelerated Fuel Capsules for Inertial Fusion Energy.

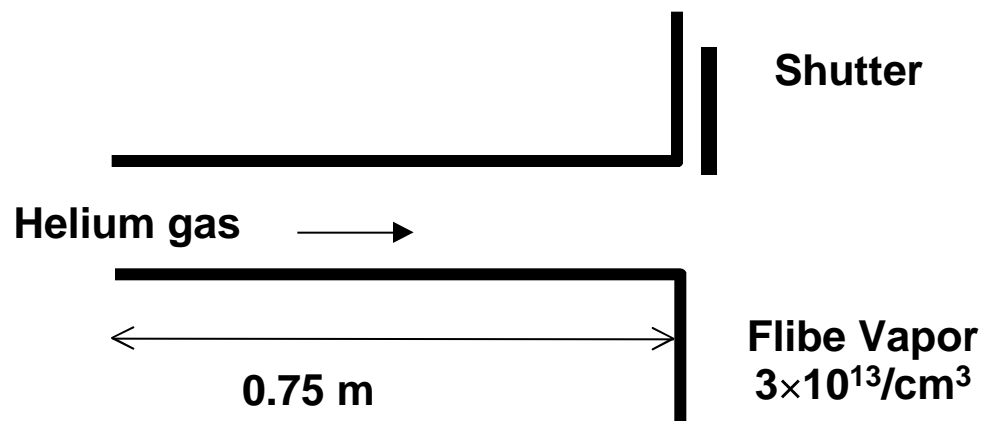
Fusion Technology, Vol. 30, Sep. 1996.

# Heating of indirect drive targets during injection is small



Heating Profile:  
300 K gas for 32 ms  
No heat load for 30 ms  
900 K chamber for 40 ms

## Counter flowing helium and shutters can minimize Flibe vapor reaching tracking system\*



2 cm opening requires ~4 Torr He with shutter open 5 ms.

Average flow rate ~0.4 mg/s.

Unabated Flibe diffusion = ~3 kg/year.

$$c = c_0 \exp - \frac{v}{D} x \quad D \sim 0.5 \text{ cm}^2/\text{s} (T/T_0)^{1.75} (P_0/P)$$

\*R. W. Petzoldt, Flibe diffusion, Unpublished memo, (2000)

# Need to demonstrate improved target tracking accuracy

1996-1998: Experimental injection and tracking experiment carried out at LBNL

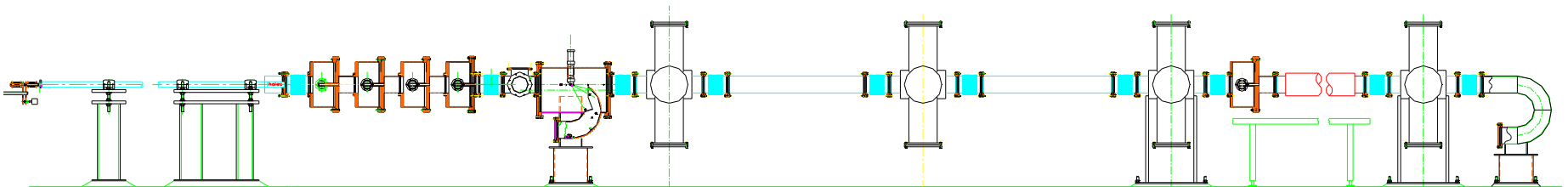
- Total transverse position prediction accuracy of  $\sigma = 160 \mu\text{m}$  achieved at 3 m distance, 70 m/s, and low repetition rate. Extrapolates to  $\sim 280 \mu\text{m}$  at 9 m.

- Current requirements:

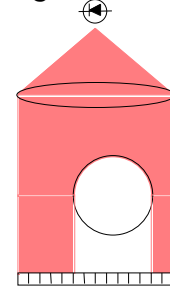
  - Up to 180 m/s and nearly all targets  $\pm 100 \mu\text{m}$  at 9 m and 6 Hz

  - Vibration isolation and multi-segment arrays are expected to improve accuracy

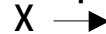
- We're building experimental system to achieve improved accuracy



Light source



Si photodiode



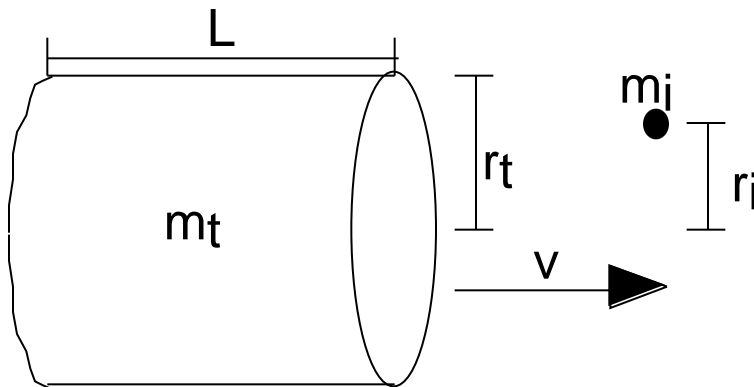
If Flibe droplet density and size are not excessive,  
in-chamber tracking should not be necessary

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$$R = \frac{v}{v_0} R_c = \frac{m_d}{m_t} R_c \implies m_d = \frac{R}{R_c} m_t = \frac{0.3 \text{ mm}}{3 \text{ m}} 2 \text{ g} = 0.2 \text{ mg}$$

Droplet radius is 0.29 mm.

Smaller droplet density is limited to about 1 g/m<sup>3</sup>.



Distance  $R_c$  from  
chamber center

Occasional verification of beam on target position may still be required.

## Summary and Conclusions

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- Targets must be strong enough for acceleration
- DT mechanical properties are being measured, others need to be
- Indirect drive target heating is calculated to be small during injection
- Gas counter flow can keep Flibe out of tracking system
- Target transverse position is measured with linear photodiode arrays.  
(Requires high speed arithmetic on pixel outputs.)

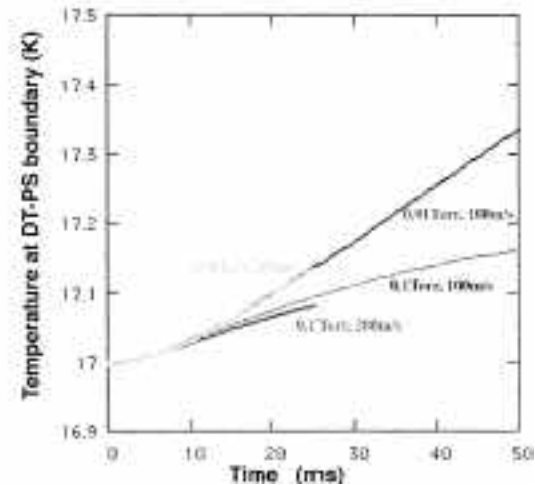
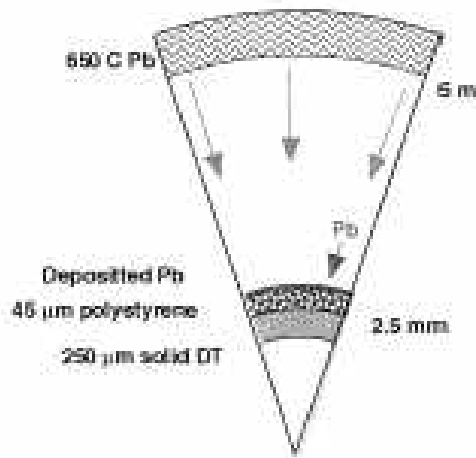


# Target heating in chamber with metal vapor

Norimatsu studied for KOYO reactor (650 C LiPb) conservatively assumed all vapor molecules that hit target stick.

Average 800 Å thick for 5 m at 200 m/s in 0.1 Torr LiPb vapor not uniform even if target spinning.

DT surface heating <0.4 K is reduced to <0.2 K by deposited metal layer.



Influence of Residual Gas on Trajectory of Injected Target  
T. Norimatsu, A. Sunahara, K. Nagai, and T. Yamanaka,  
Institute of Laser Engineering Osaka University  
Presented at the Target Fabrication meeting  
November 8-11, 199, Avalon, CA