

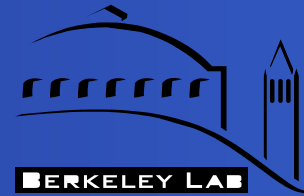
Operating Window for Channel-Assisted Pinch Propagation

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Operating window



Limits for

- chamber pressure
- chamber length
- relative density reduction

Reasons:

- energy loss of the ion beam in the channel
- channel clearance by $\mathbf{j} \times \mathbf{B}$ force
- prevent breakdown to the walls $\rightarrow n_{ch}/n_0$

Energy loss - Basics

Stopping power → Bethe formula

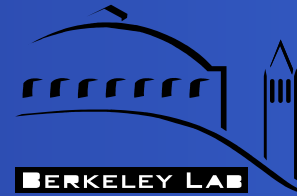
$$\frac{dE}{dx} = -\frac{1}{4\pi\epsilon_0} \left(\frac{Z_{\text{eff}} e \omega_p}{\beta c} \right)^2 \ln \left(\frac{2m_e(\beta c)^2}{I} \right)$$

Plasma frequency

$$\omega_p = \sqrt{\frac{n_{Xe} Z_{Xe} e^2}{\epsilon_0 m_e}} \rightarrow \frac{dE}{dx} \propto n_{Xe}$$

→ upper limit for chamber pressure and length

Charge state of the ion beam



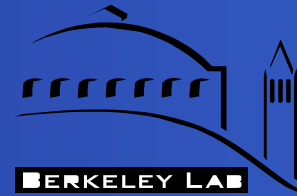
Estimated with empirical Betz formula

$$Z_{\text{eff}}(\beta) = Z_{\text{ion}} \left(1 - \exp \left[-0.555 \left(\frac{137 \beta c}{Z_{\text{ion}}^{0.517}} \right)^{1.175} \right] \right)$$

→ charge state of Pb ($\beta = 0.2$, 4 GeV)

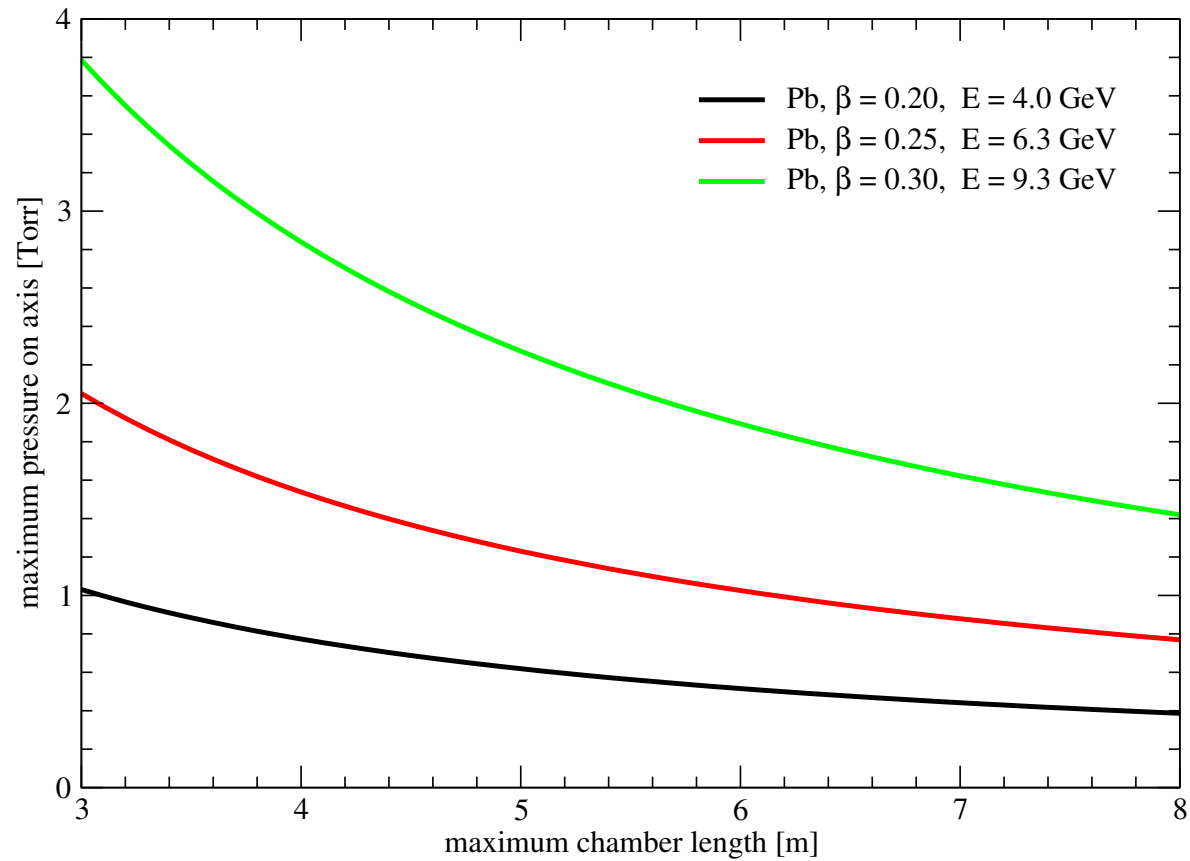
$$Z_{\text{eff}} = 69.3$$

Energy loss - results

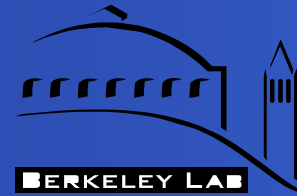


Heavy Ion beam in Xenon

Energy loss 5%



Channel clearance



Ion beam induces return current $\rightarrow \mathbf{j} \times \mathbf{B}$ force

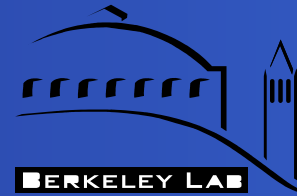
$$\rho \frac{d\mathbf{v}}{dt} = -\nabla p + \mathbf{j} \times \mathbf{B}$$

\rightarrow lower limit for gas density on axis

Estimate: neglect pressure term

$$\Delta x = \left(\frac{\mu_0 I_{\text{beam}} I_{\text{net}}}{4\pi^2 R_0^3 \rho} \right) t^2$$

Lower bound for density



Example:

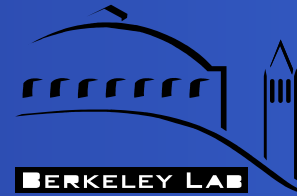
$I_{\text{net}} = 50 \text{ kA}$, $I_{\text{beam}} = 3 \text{ MA}$, $R_0 = 5 \text{ mm}$, $t = 10 \text{ ns}$,
 $\Delta x \leq 1 \text{ mm}$:

$$\rho \geq 3.8 \cdot 10^{-3} \text{ kg/m}^3 \text{ (0.5 Torr)}$$

Better calculation:

- expansion slowed down by wall of increased gas density \rightarrow smaller limit
- hydrodynamical simulation necessary

Breakdown



Breakdown condition for xenon:

$$(E/p)_{Xe} = 60 \text{ V}/(\text{cm Torr})$$

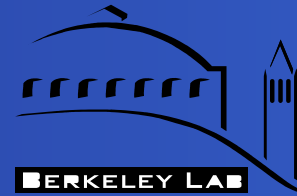
Prevent breakdown to chamber wall:

$$(E/p)_{\text{channel}} > (E/p)_{Xe} \text{ and } (E/p)_{\text{chamber}} < (E/p)_{Xe}$$

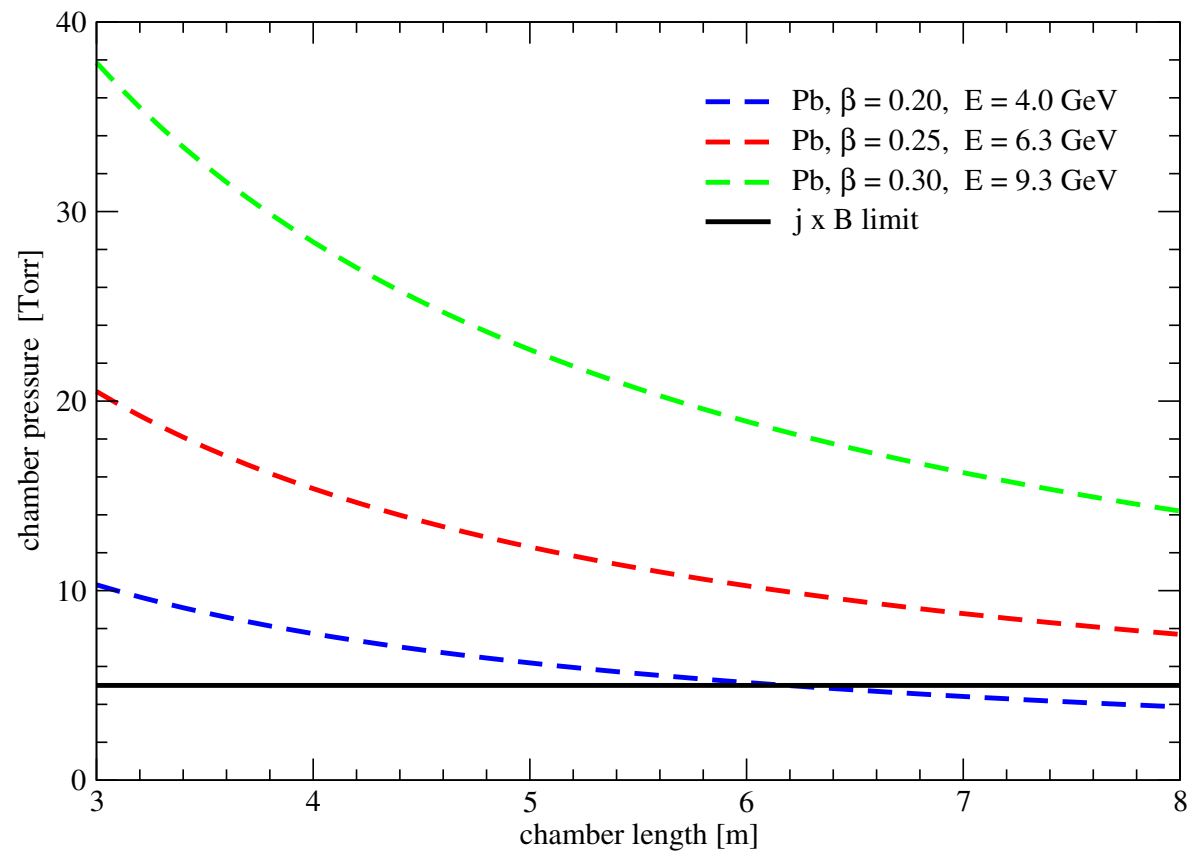
→ criterion for rarefaction:

$$\frac{n_{\text{channel}}}{n_{\text{chamber}}} < \frac{R_{\text{port}}}{R_{\text{chamber}}} \approx 0.1$$

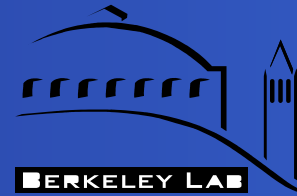
Resulting operating window



Energy loss 5%, channel rarefaction 10%



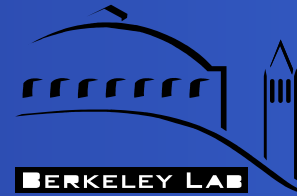
Simulation



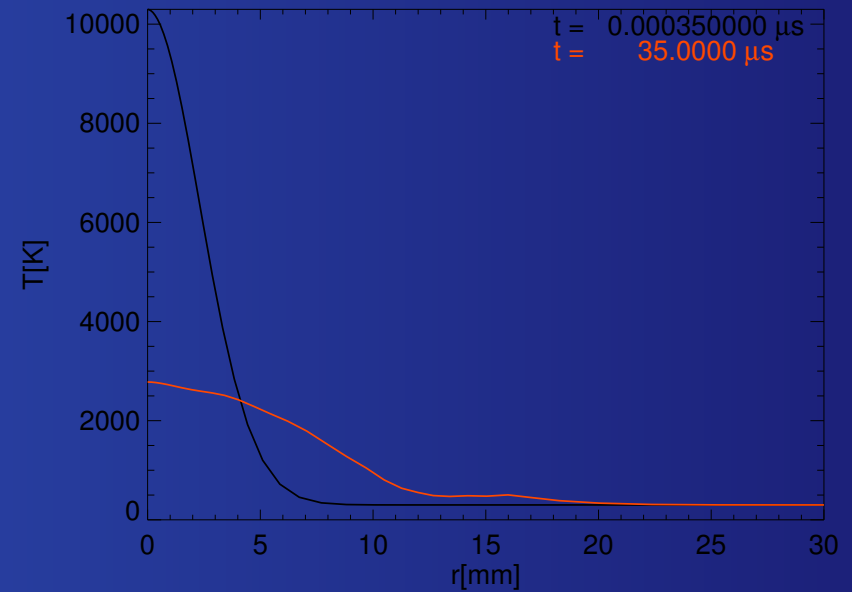
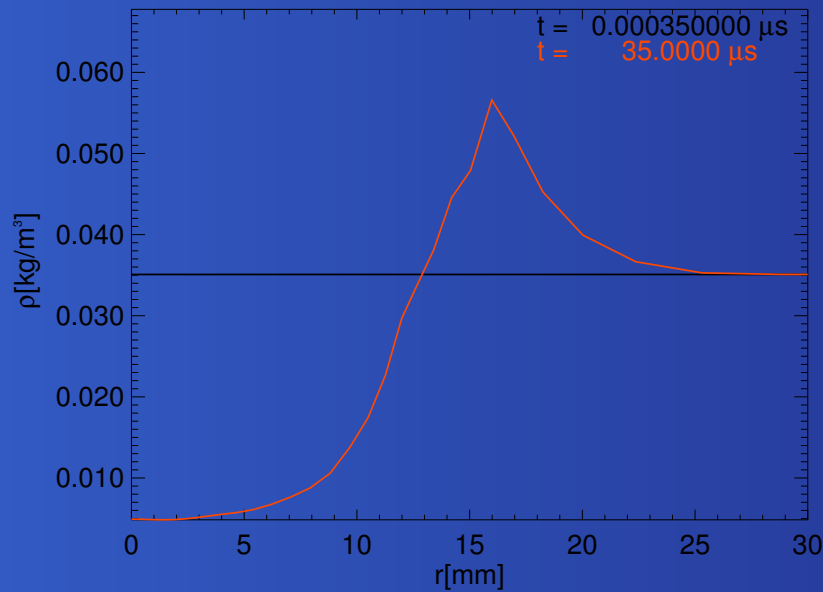
Critical point: rarefaction on axis achievable ?

- hydrodynamical simulation code Cyclops
 - cylindrical symmetry → one spatial dimension
 - lagrangian formulation
 - thermal conductivity and other properties calculated with fits to measured values
- compare with measurements and analytic models

Simulation results

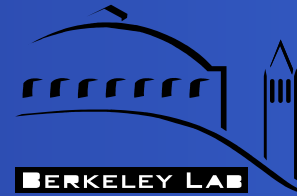


5 torr xenon, no thermal conduction

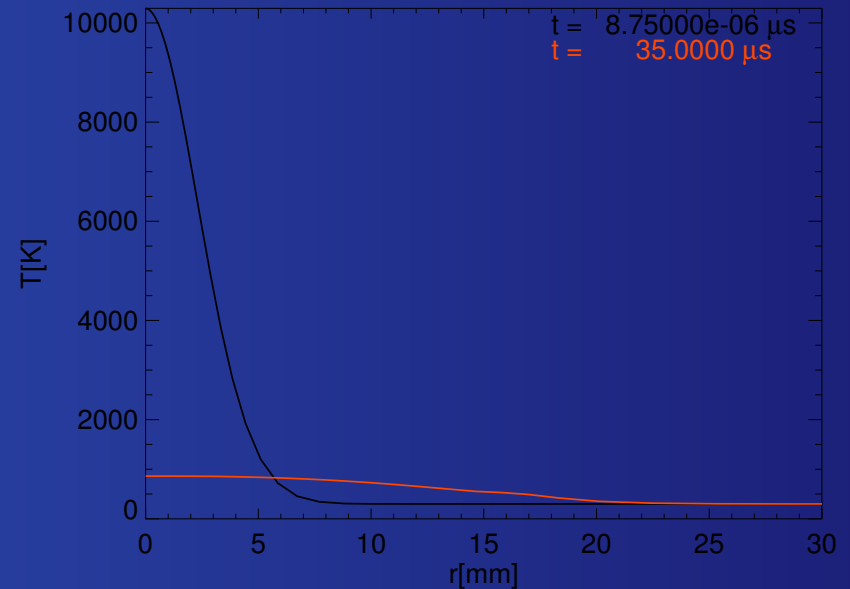
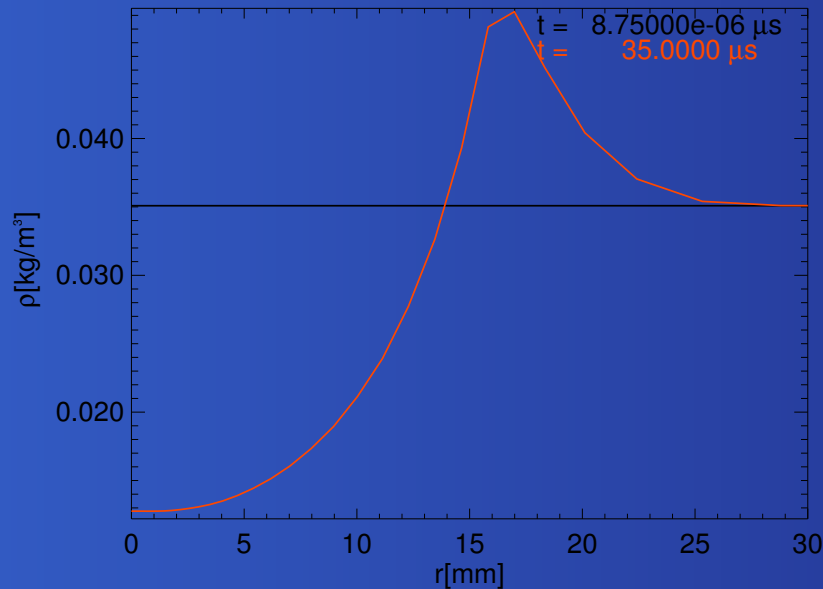


10,000 K lead to $n_{\text{ch}}/n_0 = 14\%$

Simulation results II

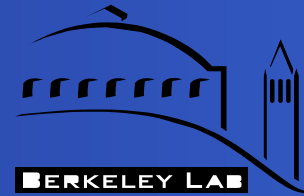


5 torr xenon, with thermal conduction



10,000 K only lead to $n_{\text{ch}}/n_0 = 34\%$
→ effect of thermal conduction too large

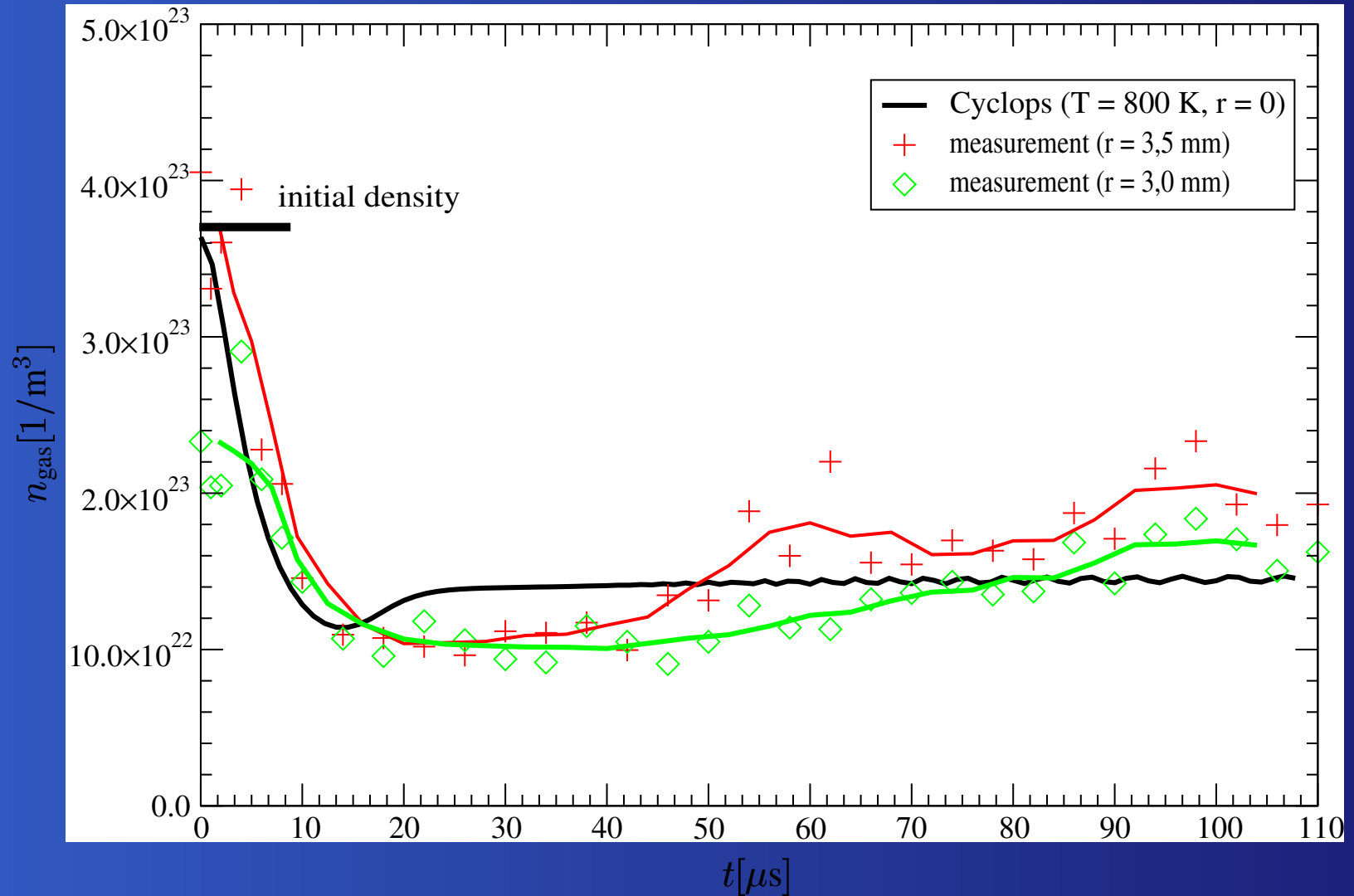
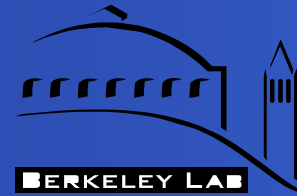
Density measurements



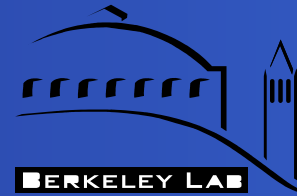
Measurements were performed at GSI z-pinch experiment

- density was determined by the scattering of a heavy ion beam
- applicable to hydrodynamic expansion but not for discharge
- experiments with ammonia: good agreement between measurement and simulation
- could be applied for xenon discharge

Measurements in ammonia



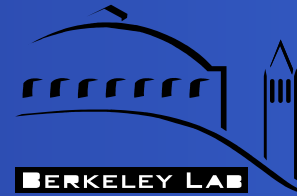
Analytical channel model



Assumptions

- starting with continuity equation and force equation
- homogeneous current density inside channel
- surrounding gas is neglected

Averaged values



Calculate moments \rightarrow integrate over radius

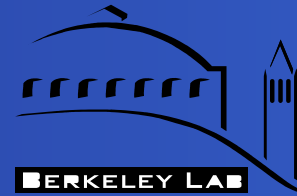
- mass line density

$$N = 2\pi \int r \rho dr = \pi R_0^2 \rho_0$$

- averaged radius

$$R^2 = \langle r^2 \rangle = \frac{2\pi}{N} \int r^3 \rho dr$$

Envelope equation

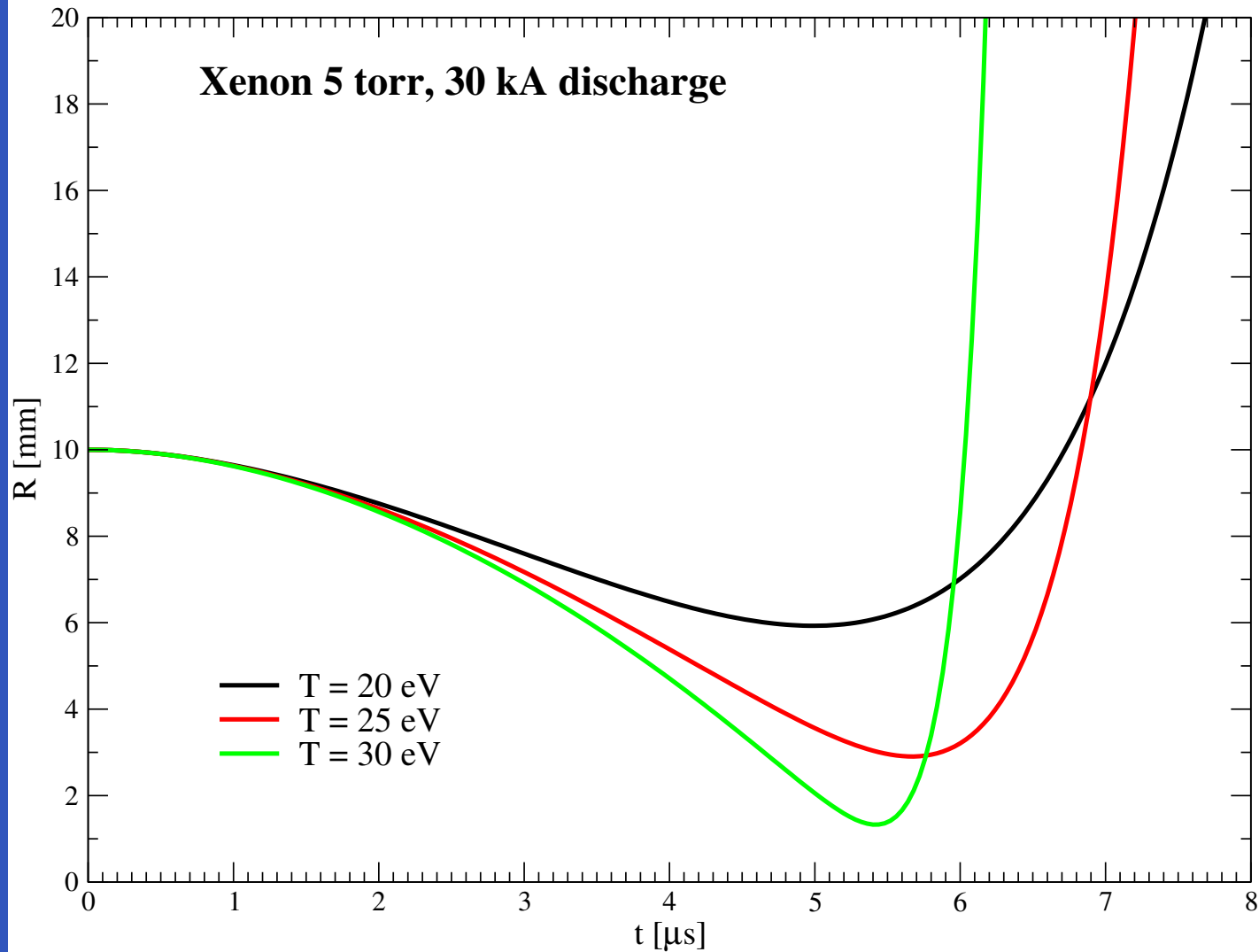
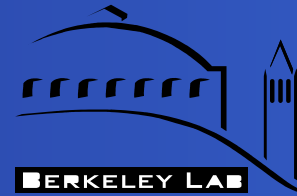


Integrating the force equation yields

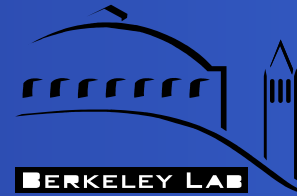
$$\frac{d^2 R}{dt^2} = \frac{c_1}{NR^3} - \frac{c_2 I^2}{NR} + \frac{c_3 R}{N} \left(\int_0^t \frac{I^2(\tau)}{R^4(\tau)} d\tau \right)$$

- can be solved numerically (for constant current)
- compare with calculated moments from Cyclops runs (yet to be done)

Example – varied conductivity



Conclusions/Outlook



- calculations indicate good operating window
- MHD simulation of channel clearance necessary
- gas rarefaction is a critical point:
 - model for thermal conduction needs to be checked
 - analytical model useful for comparison
 - comparison with measurements