

# Stellarator magnet conductors

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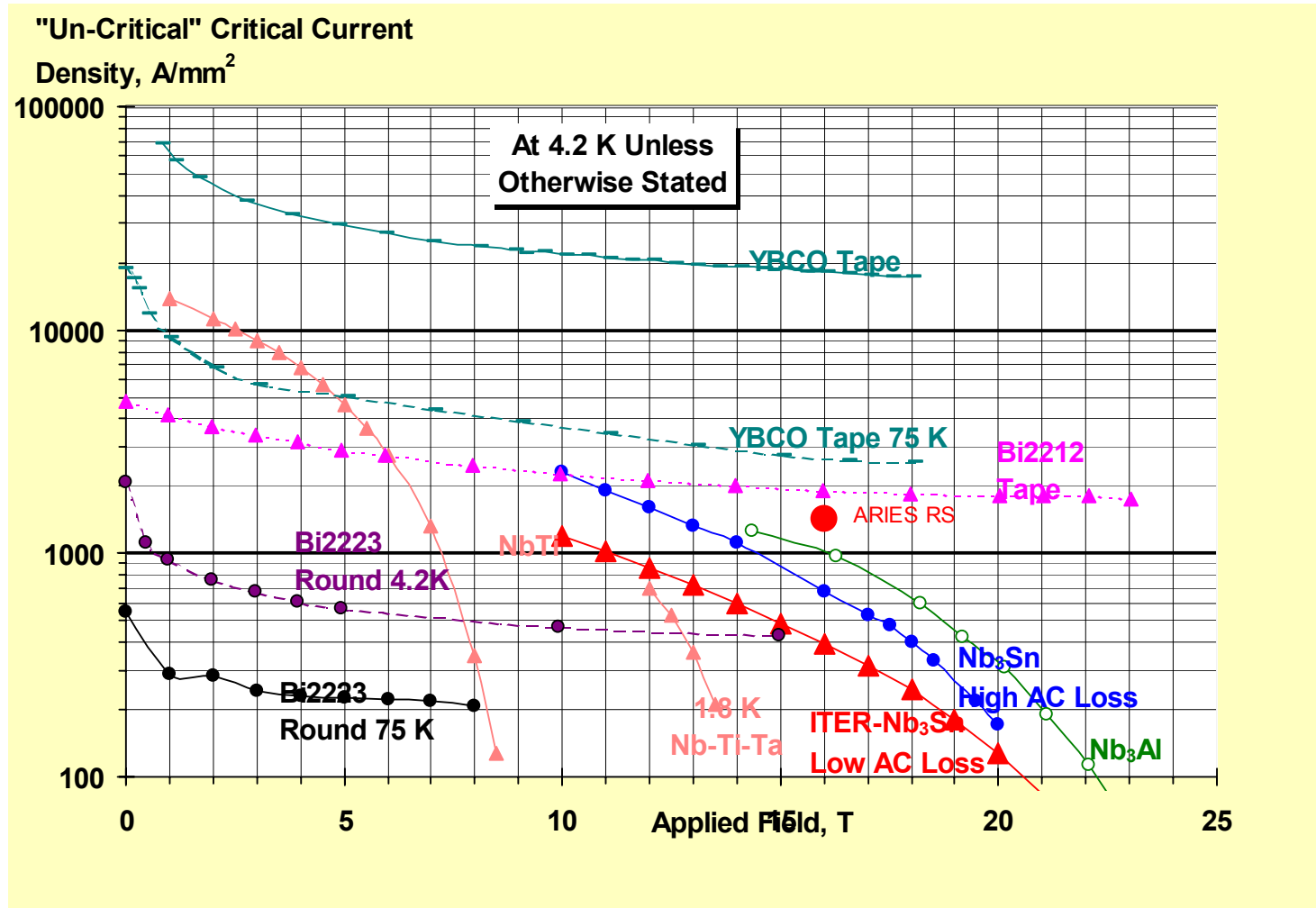
Aries Meeting, Georgia Tech

September 3, 2003

# Organization of talk

- Status of HTS/comparison with LTS
- Design optimization of LTS
- Cost comparison

# HTS Superconductor options and comparison with LTS (YBCO tape at 4 K and at 75 K)

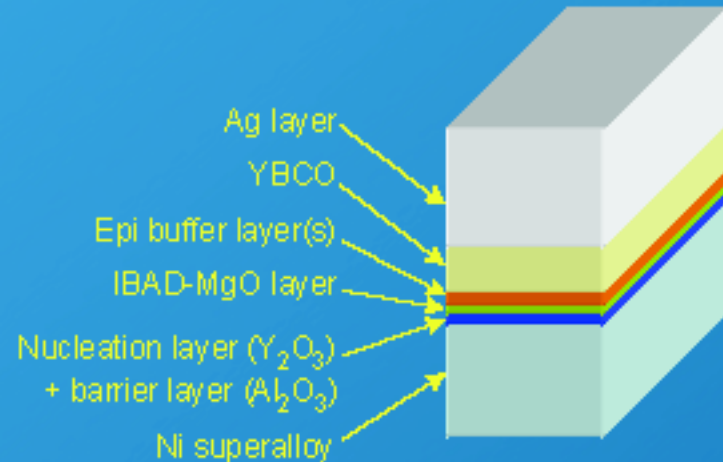


# Status of industry

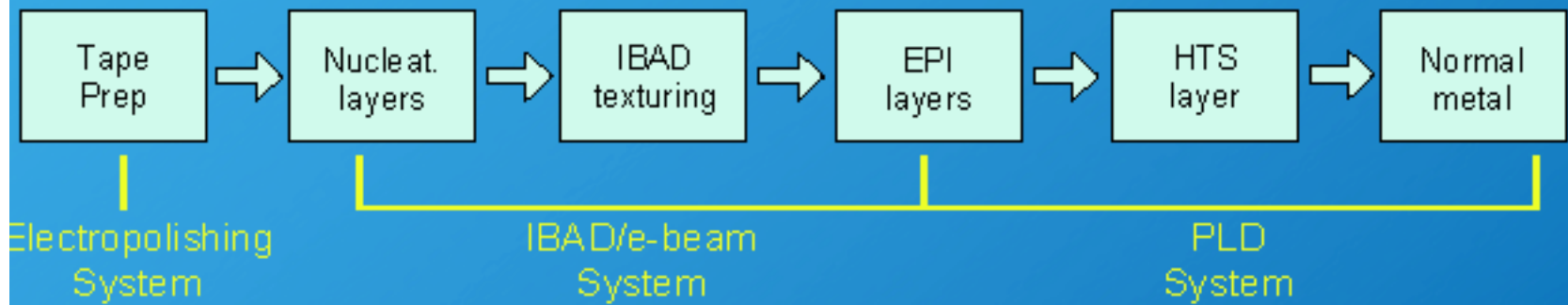
- Japan/US/EU continue to support industry
  - In US, mainly for power applications (motors, generators, fault limiters, transmission lines)
- In the US, American Superconductor
  - Dropping all but YBCO
  - Hopes to hit 10-20 \$/kA m (competitive with copper)
- Japan, Europe supporting others (2212)

# LANL Coated Conductor

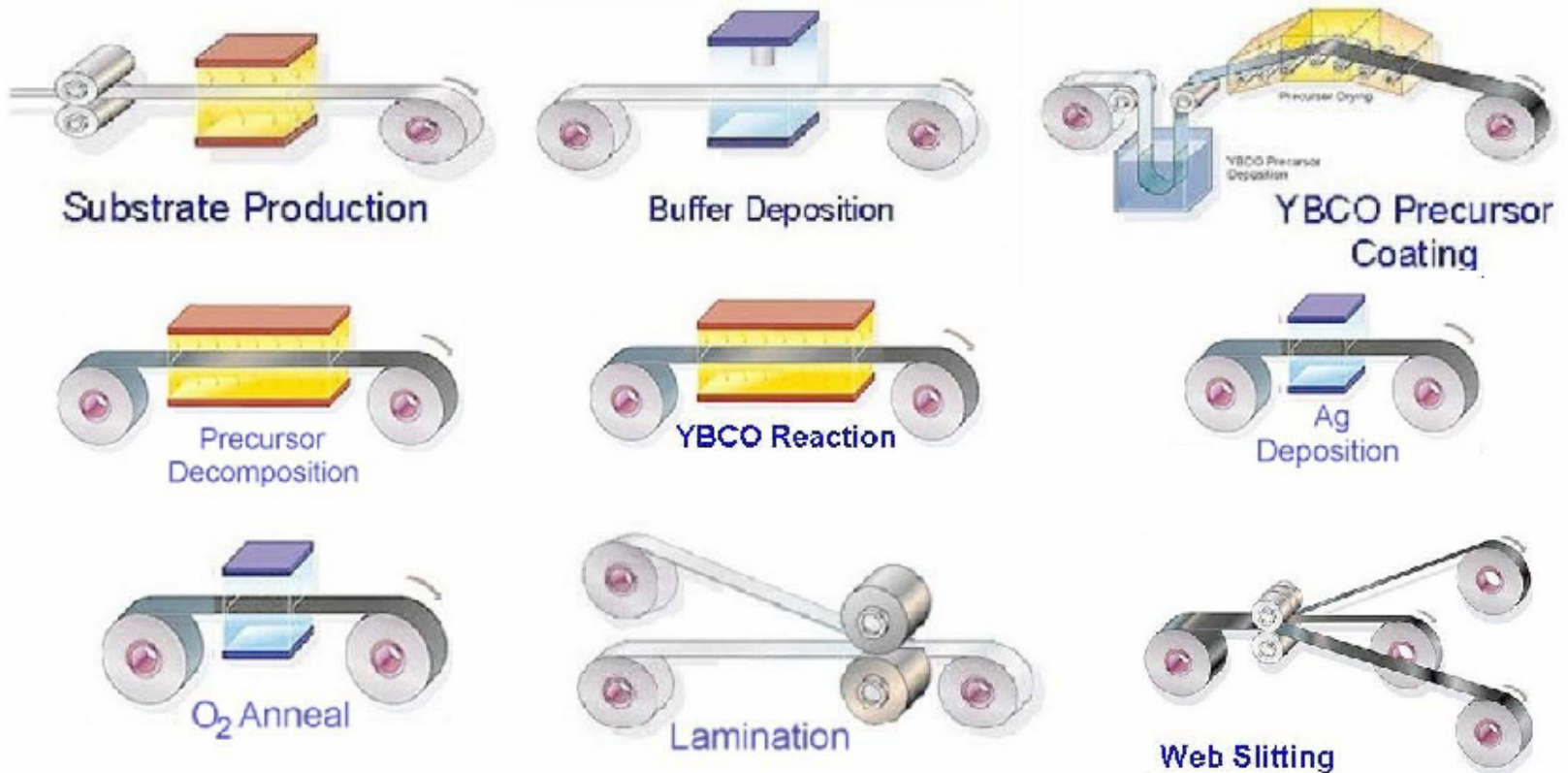
- IBAD-textured MgO template on a Ni-superalloy
  - IBAD layers deposited by e-beam evaporation at RP
- Pulsed-laser deposited buffers and superconductor



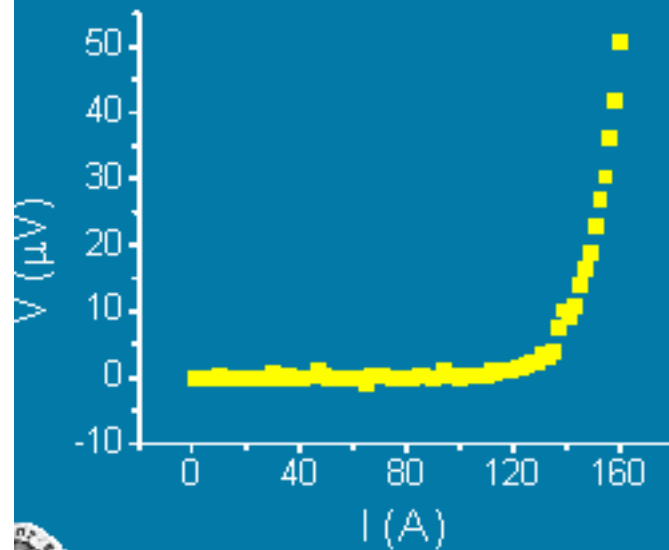
Los Alamos Research Park:



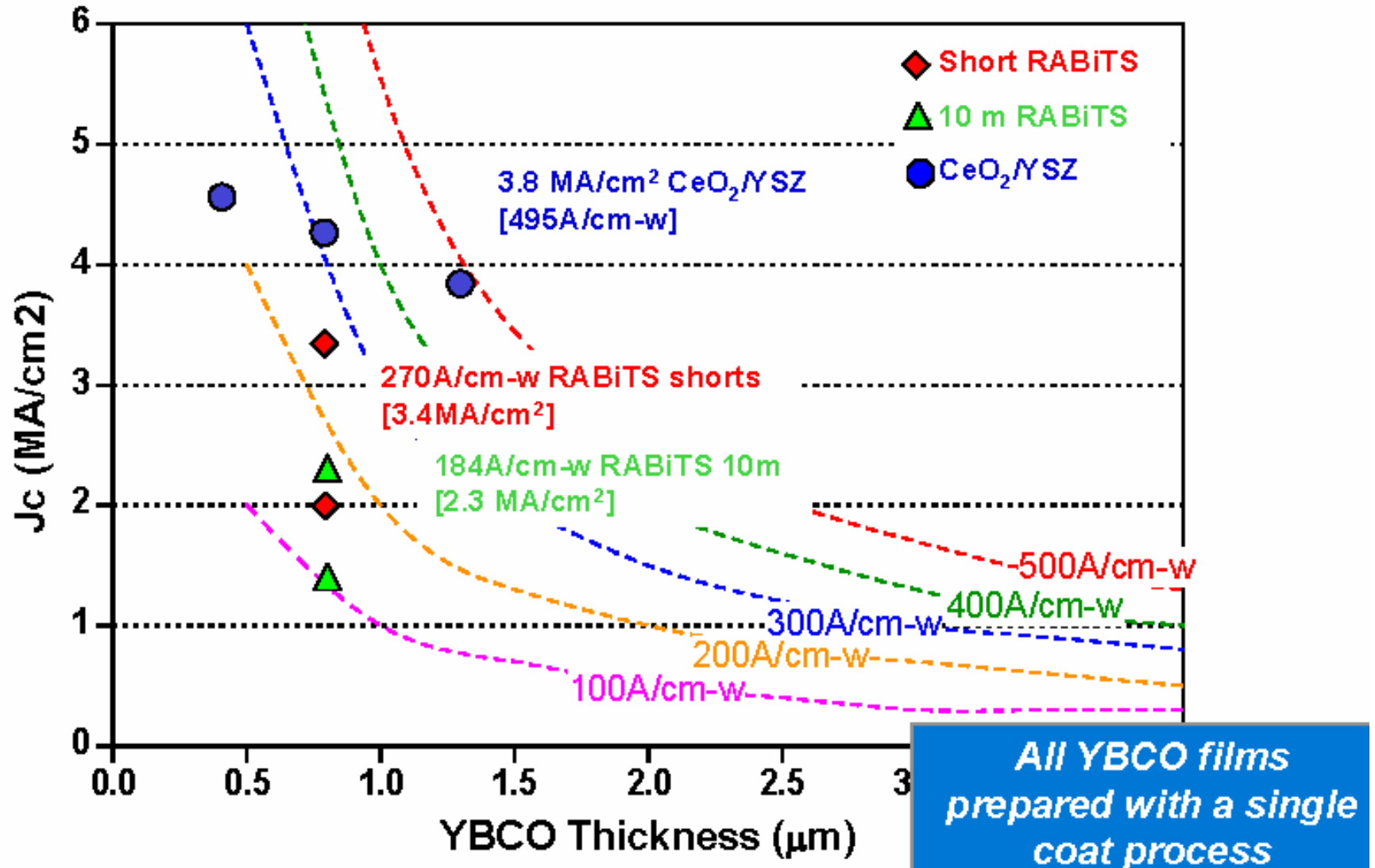
# AMSC current 2G wire process (scaleable to 10cm wide web which yields 20 4mm wires)



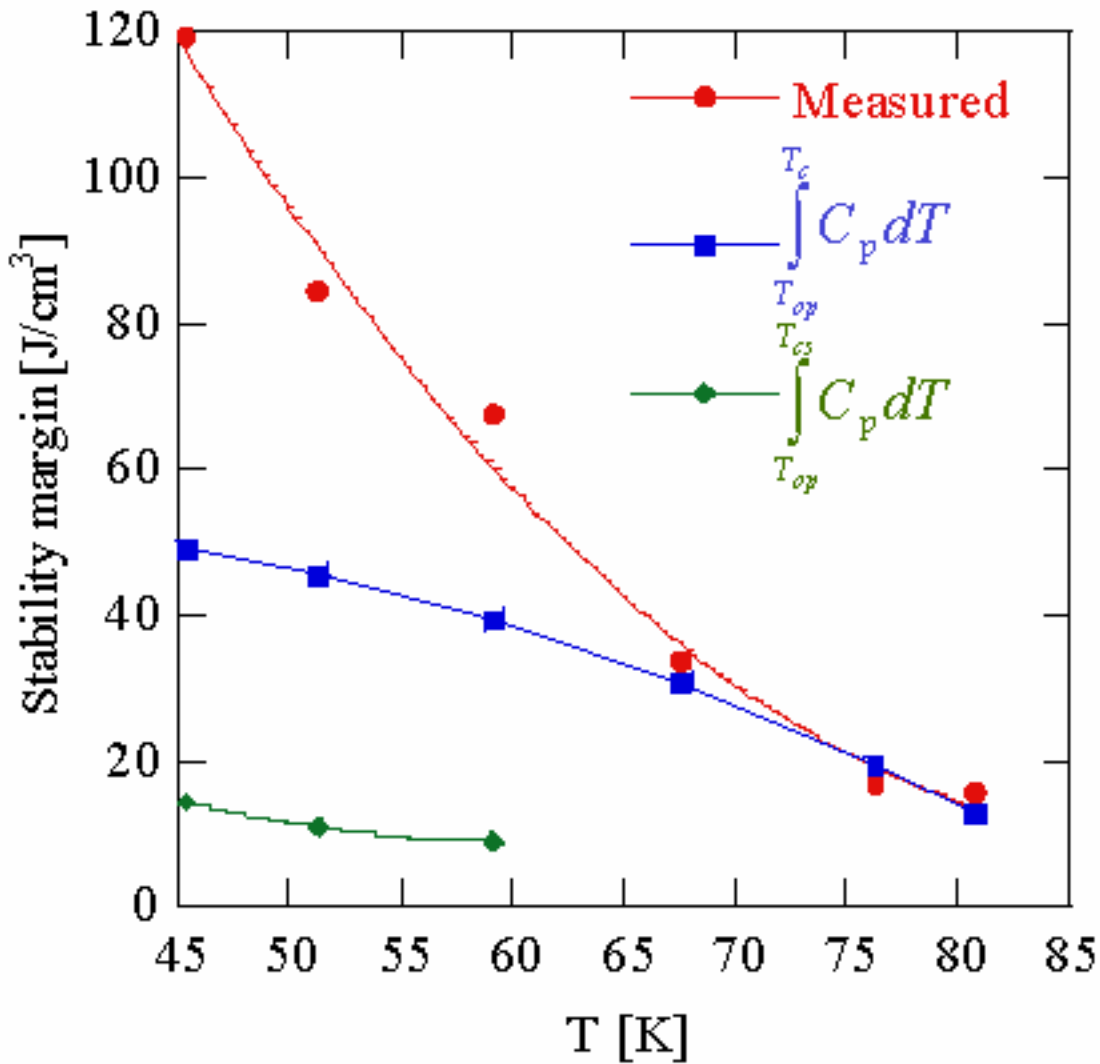
- 2  $\mu\text{m}$  YBCO/50 nm LMO/Epi-MgO/IBAD-MgO/Nickel alloy
  - 178 A across 1 cm
  - 120 A across 10 - 20 cm
  - 50 A across 1.1 m
  - Microbridges - 1.1 MA/cm<sup>2</sup>



# AMSC, ORNL conductor development

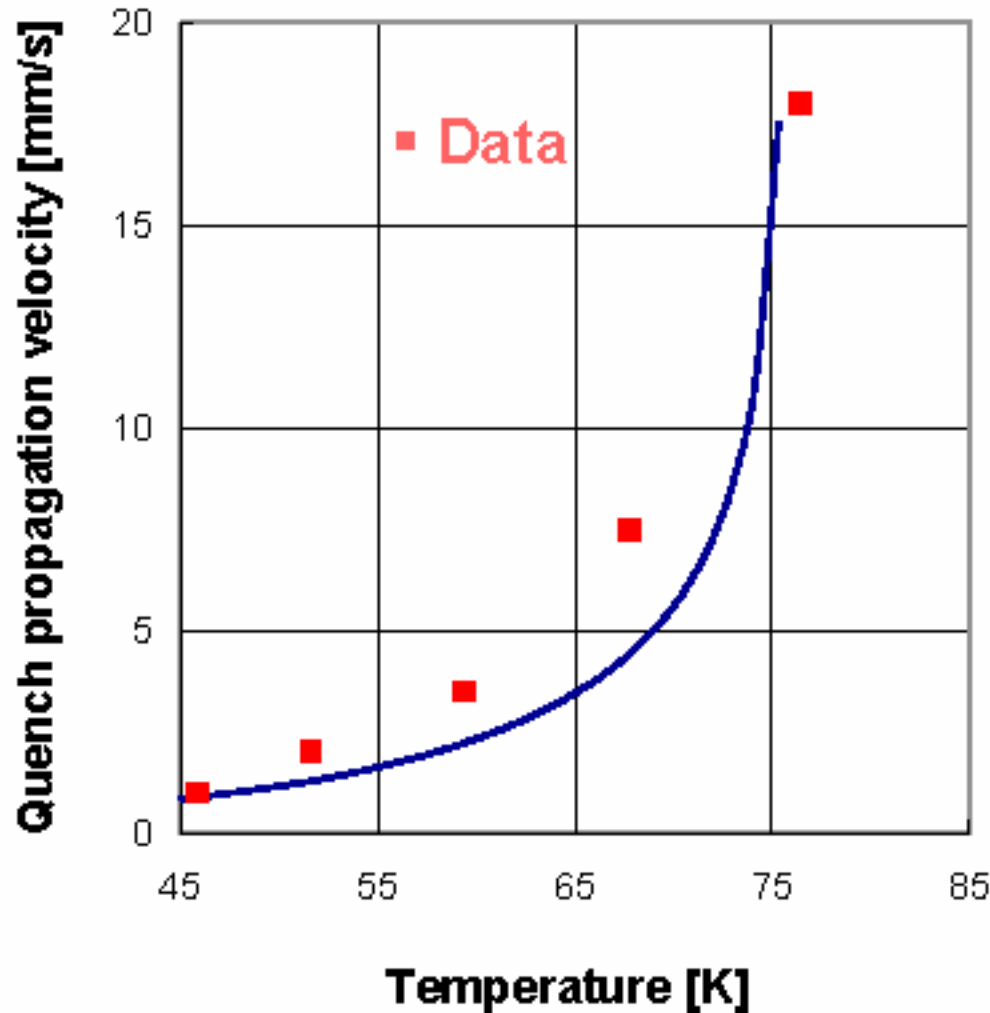






Stability margin for low Tc superconductors  $\sim$  100's mJ/cm<sup>3</sup> (3 orders of magnitude smaller)

# Quench propagation



For low  $T_c$ ,  
quench  
propagation  
velocity is  $\sim 10$   
m/s (3 orders of  
magnitude  
larger)

# Stabilizer

- In order to allow for proper cooling of HTS in region of poor superconductivity, M. Gouge recommends 5 mΩ/m resistive shunt (7/03)
- This decreases substantially the current density

Desired minimum resistivity	5.00E-03 Ohm/m
Copper resistivity @ 77 K	2.57E-09 Ohm m
Width	0.01 m
Thickness	5.14E-05 m

- For ARIES-stellerator: no shunt material, beyond that required for manufacturing

# HTS conductor current density

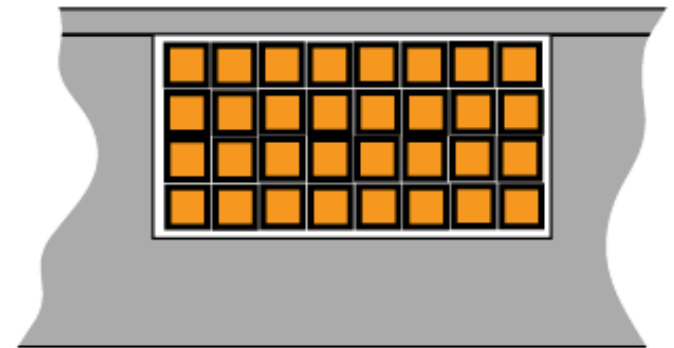
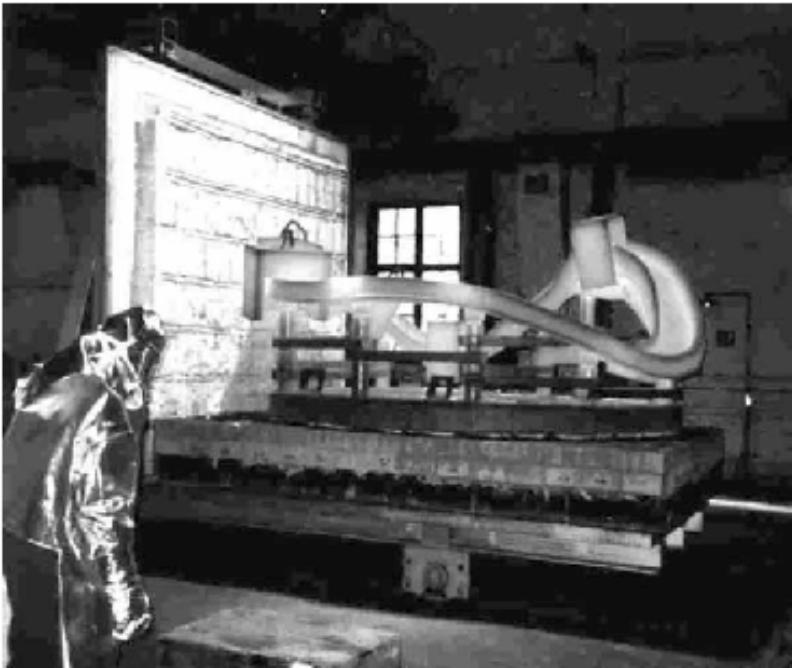
- YBCO and related 123 materials have texturing issues that decrease current density with thickness.
- Thickness of superconductor is  $\sim 1$ -2 microns
- Thickness of structure (Ni-based materials, either Ni, NiW or Hastelloy) is  $\sim 400$ -500 microns.
- Current density in conductor is 2 orders of magnitude smaller than superconductor
- But
  - Likely that SC can be deposited in much thinner substrates
  - If 50 microns, drop in current density only 1 order of magnitude

# HTS as of 7/03

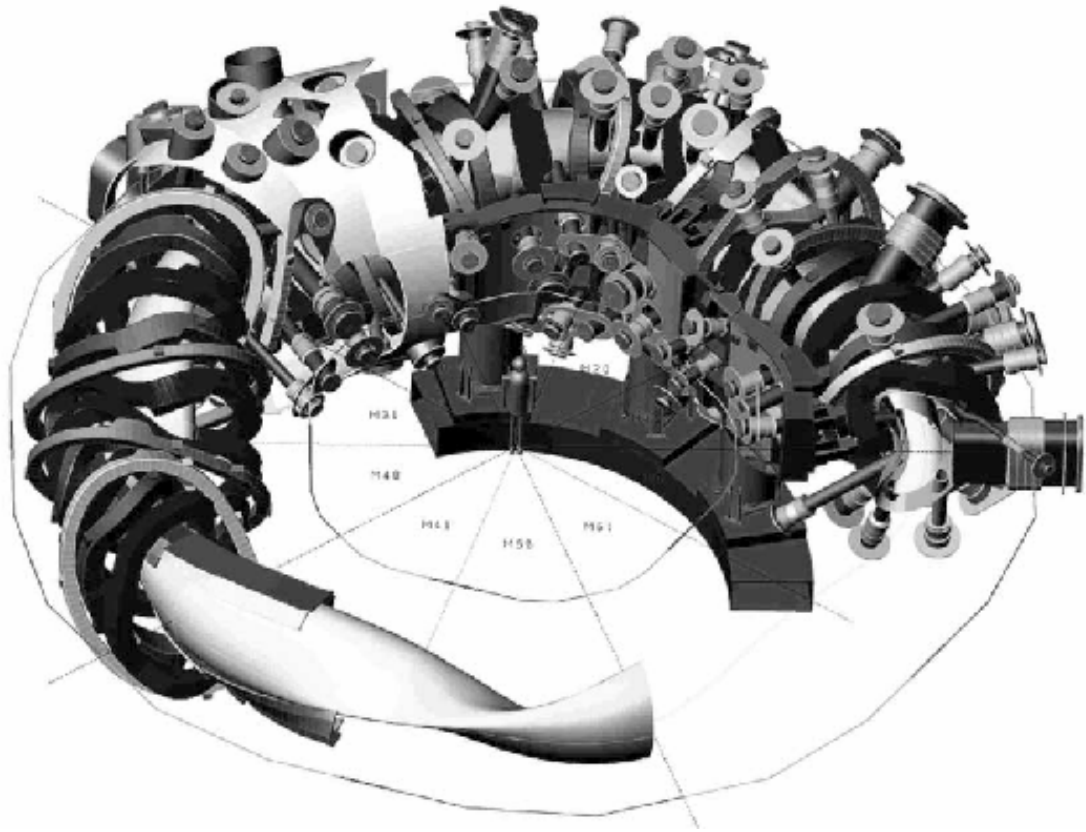
- Dependence of properties on YBCO thickness
  - $J_c \sim 1/d^{1/2}$
  - $I_c \sim d^{1/2}$
- The best YBCO result to date (77 K)
  - for thick (2.9  $\mu\text{m}$ ) on IBAD-YSZ  $I_c \sim 270$  A/cm
  - reel-to-reel RABiTS, 188 A/cm is for a 2.4- $\mu\text{m}$ -thick coating, although one 1.37- $\mu\text{m}$ -thick film exhibited an  $I_c = 219$  A/cm, in 10 m long section
- Best properties for YBCO at 77K:
  - $J_c \sim 2$  MA/cm<sup>2</sup> in 0.35- $\mu\text{m}$ -thick for IBAD-MgO.
  - $J_c \sim 3$  MA/cm<sup>2</sup> in 0.9 $\mu\text{m}$  for RABiTS

# ARIES-Stellarator magnet concept

- For assembly/maintenance, Mallang proposes structural trenches where conductor is inserted



# Magnet structure concept



Instead of individual forms for magnet structure, shells with trenches used for structure

Wendelstein 7-X

# Low temperature magnet

- Use grading to decrease cost
  - Use NbTi in regions of low field ( $< 7$  T)
  - In regions of higher field, use Nb<sub>3</sub>Sn or equivalent
- Problem:
  - To wind stellerator magnets with Nb<sub>3</sub>Sn, it is needed to use react and wind method
  - Magnets too complicated for applying insulation/bonding after winding (wind & react)
- Solution: Use high T<sub>c</sub> material at low T<sub>c</sub>



# High Tc (at low temperature)

- Justin Schwartz (ARIES-1), now at FSU HFNML (Tallahassee, FL)
  - **It all started here (actually, in UCLA)!!!**
- Record field, energy, number of turns
  - BSCCO 2212

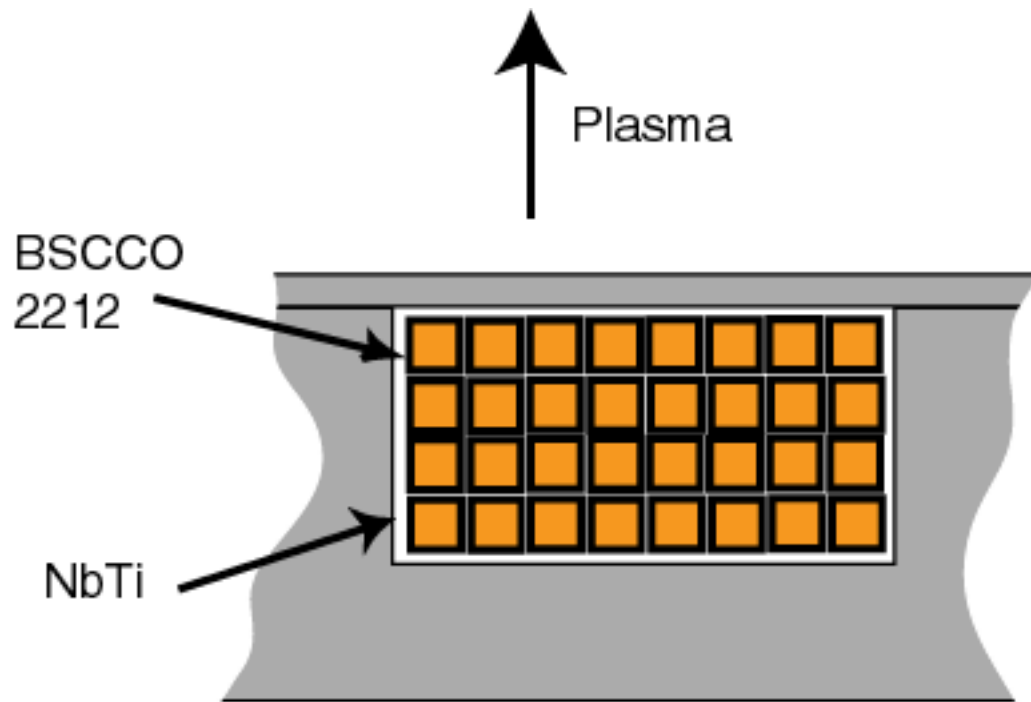
HTS insert	Background	Total
5.19	18	23.19
5.13	19	24.13
5.08	19.94	25.02

# Oxford/NHMFL HTS insert BSCCO 2212



“Fusion should not have to wait  
for High Temperature  
Superconductor”

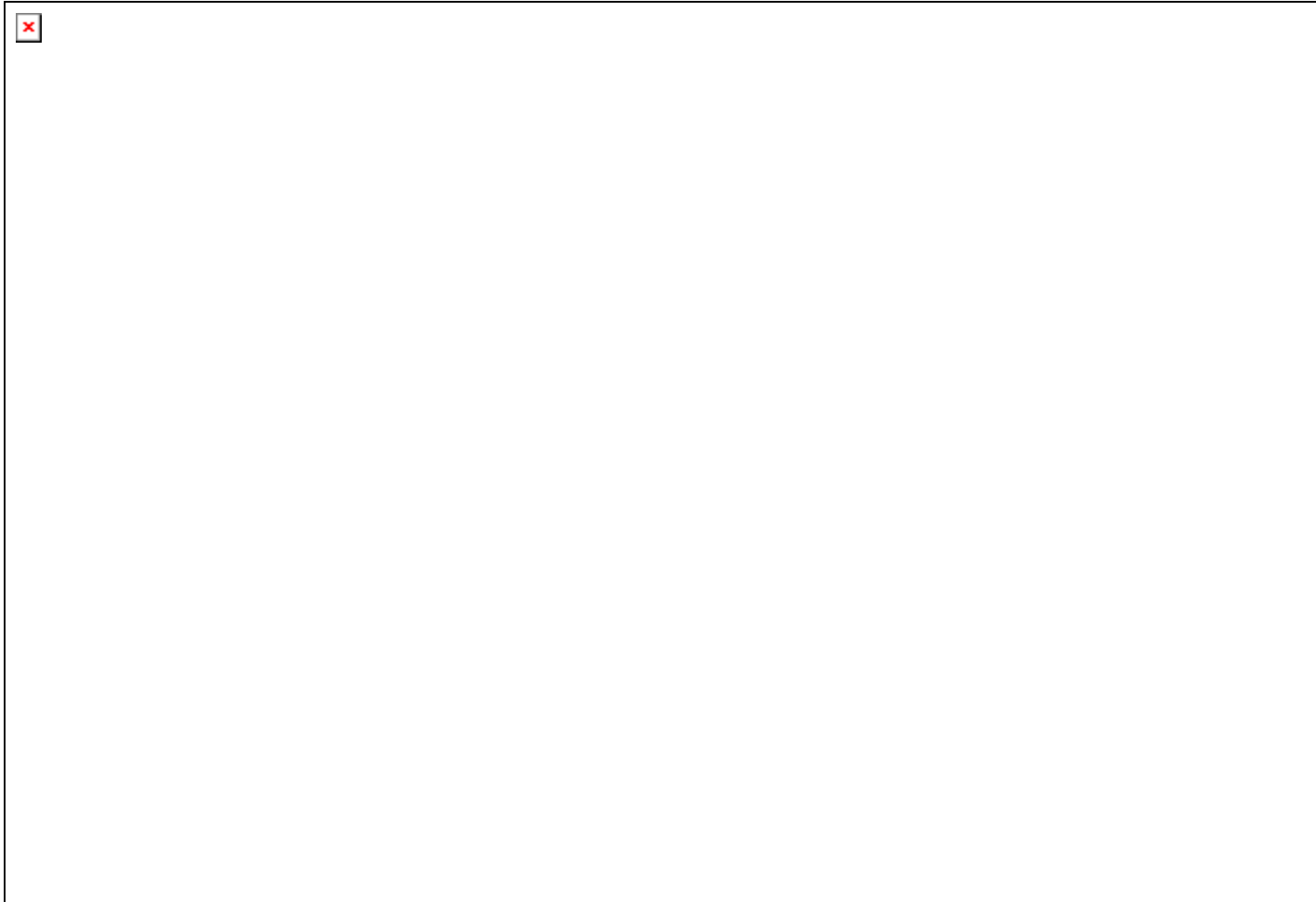
*Comment made by a leader of the magnet fusion technology  
activity to Justin Schwartz*



# LTS design of conductor

Magnetic field	T	10	12
SC current density	A/m <sup>2</sup>	4.00E+09	3.00E+09
J2 tau	(A/m <sup>2</sup> )s	5.00E+16	5.00E+16
tau	s	2.00E+00	2.00E+00
Current density in Copper	A/m <sup>2</sup>	2.24E+08	2.24E+08
Helium fraction		0.25	0.25
Sheathing thickness			
B <sup>2</sup> /2mu0	Pa	3.98E+07	5.73E+07
Stress in sheath	Pa	8.00E+08	8.00E+08
Fractional thickness of sheath		4.97E-02	7.16E-02
Sheath fraction in conductor		9.70E-02	1.38E-01
Current density	A/m <sup>2</sup>		
Current density in strands	Conductor	2.12E+08	2.08E+08
Strands + Helium	Conductor + helium	1.59E+08	1.56E+08
Strands+helium+sheath	Conductor + Helium + sheath	1.43E+08	1.35E+08

# LTS conductor design



# Current density in LTS

- In 5/7 meeting, I mentioned that winding pack current density could be as high as 300 MA/m<sup>2</sup>
- More careful investigation (*i.e.*, inclusion of quench protection), reduces current density to about 100 MA/m<sup>2</sup>

# Cost comparison

- NbTi
  - Presently: 1-2 \$/kA m
- Nb<sub>3</sub>Sn
  - Today: 10-20 \$/kA m
  - Expected: 2-4 \$/kA m
- YBCO
  - Presently: 200 \$/kA m
  - Guessed: 10-20 \$/kA m
  - Expert opinion: 50\$/kA m

# Magnet design algorithms

- This presentation provides algorithm for LTS design, modified for stellerator applications
  - Winding of conductor in trench, with substantial strains ( $\text{Nb}_3\text{Sn}$  can not be used)
  - Conductor grading: NbTi in low field region, BSCCO 2212 in high field region
  - Costing for LTS and HTS
- Model for HTS in January presentation:  
[aries.ucsd.edu/ARIES/meeting/0106/bromberg.pdf](http://aries.ucsd.edu/ARIES/meeting/0106/bromberg.pdf)
- Model for structure in May meeting:  
[aries.ucsd.edu/ARIES/meetings/0507/bromberg.pdf](http://aries.ucsd.edu/ARIES/meetings/0507/bromberg.pdf)