

Neutron Wall Loading Profile Using CAD/MCNP Interface

Mengkuo Wang

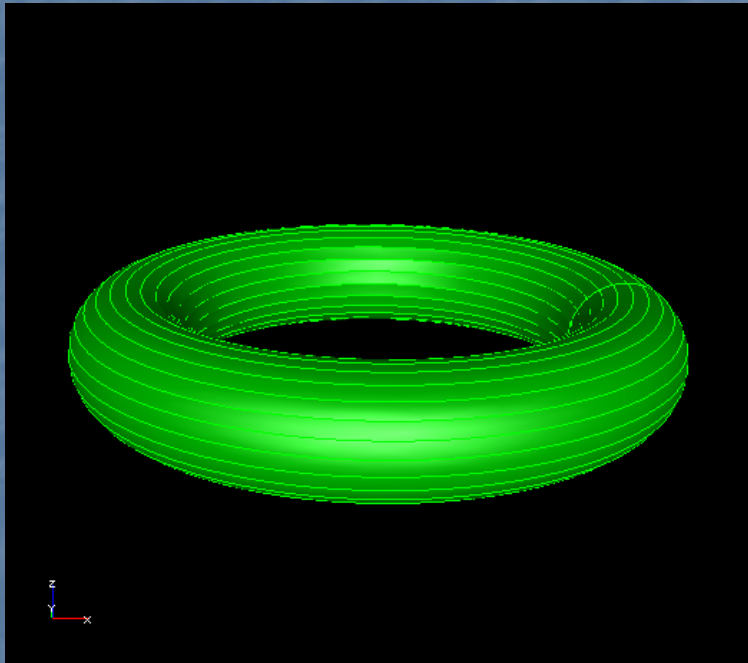
ARIES Meeting

Sep 16, 2004

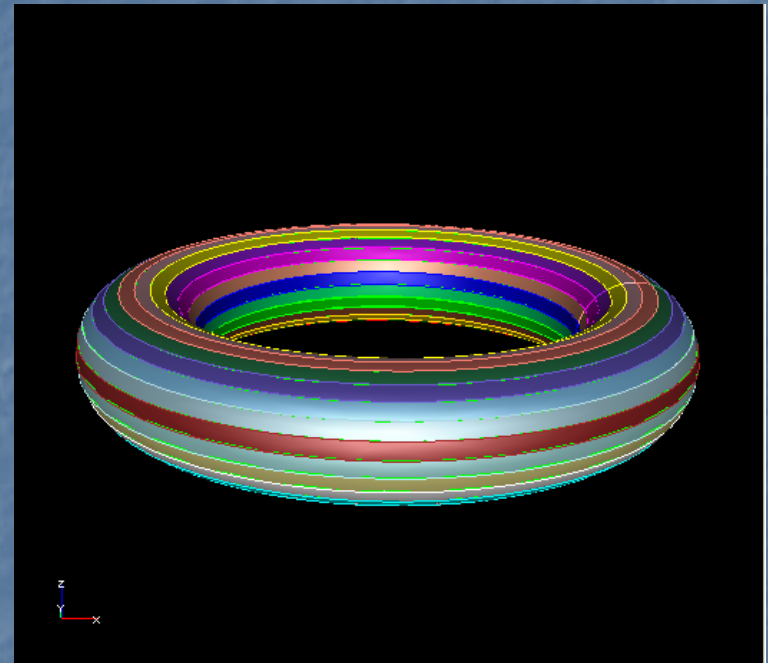
University of Wisconsin - Madison

(Last time) First step: torus

Plasma Surface

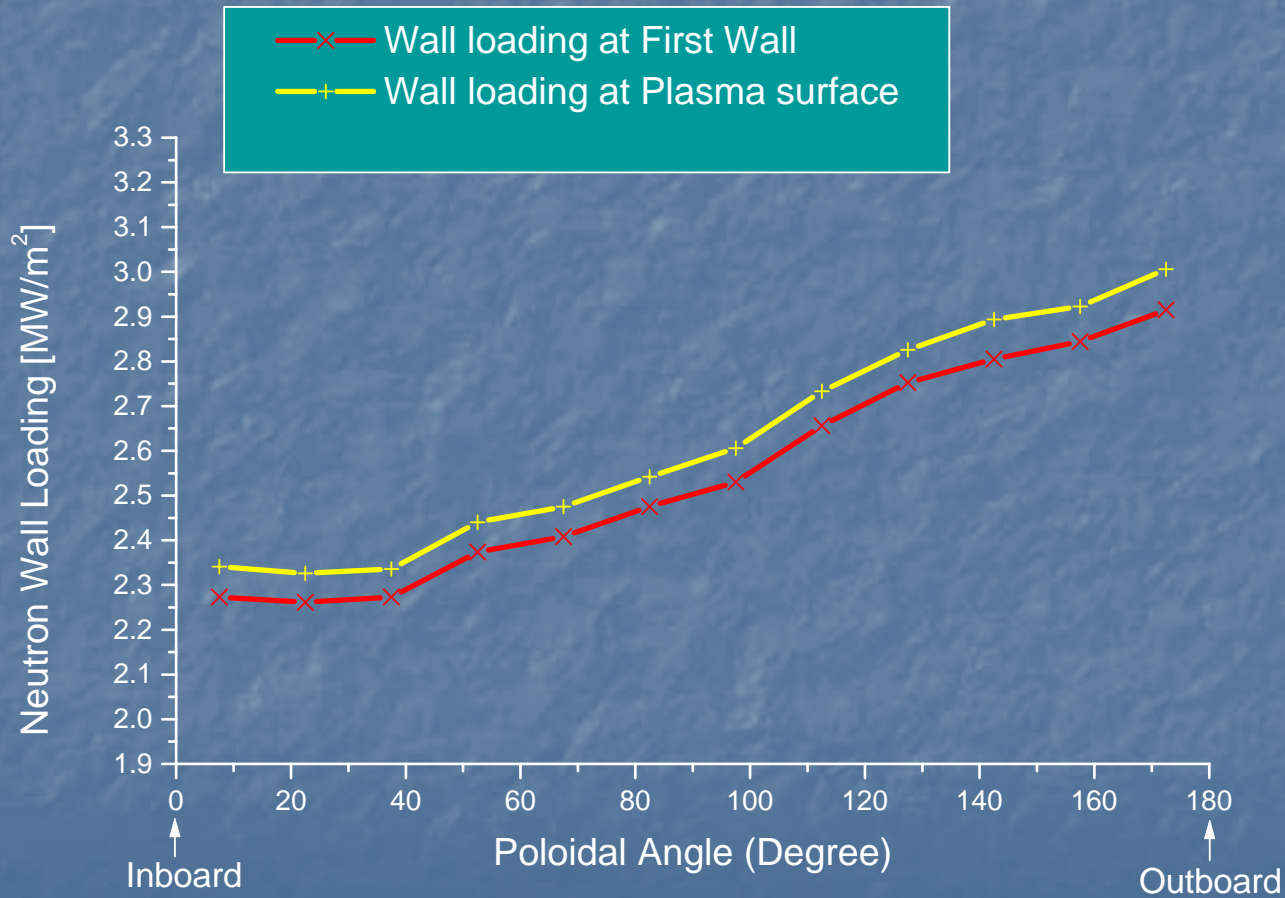


First Wall



First Wall divided poloidally
into 15 degree bins

(last time) Result Differ by $\sim 3\%$ for 5cm SOL

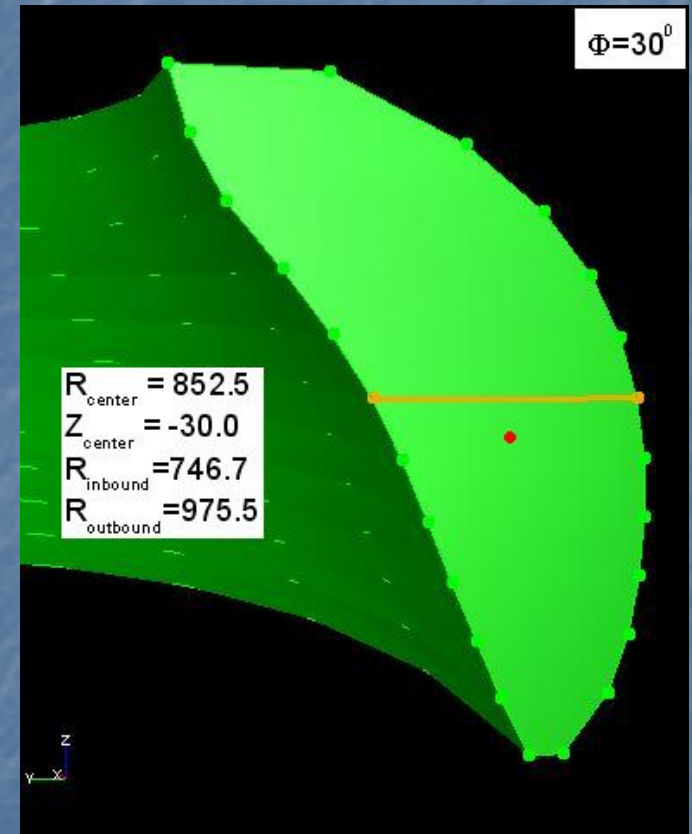
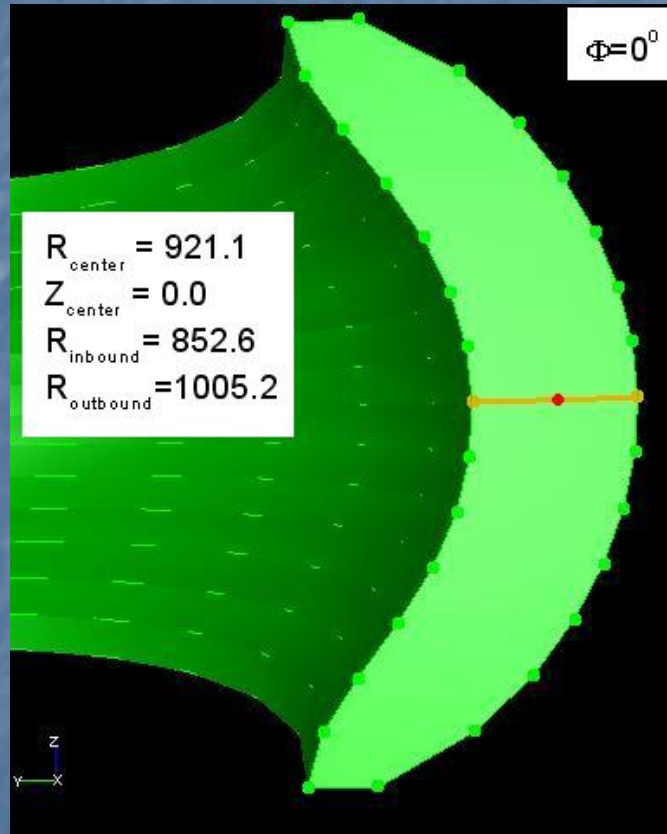


(last time) Wall subtract Plasma Surface

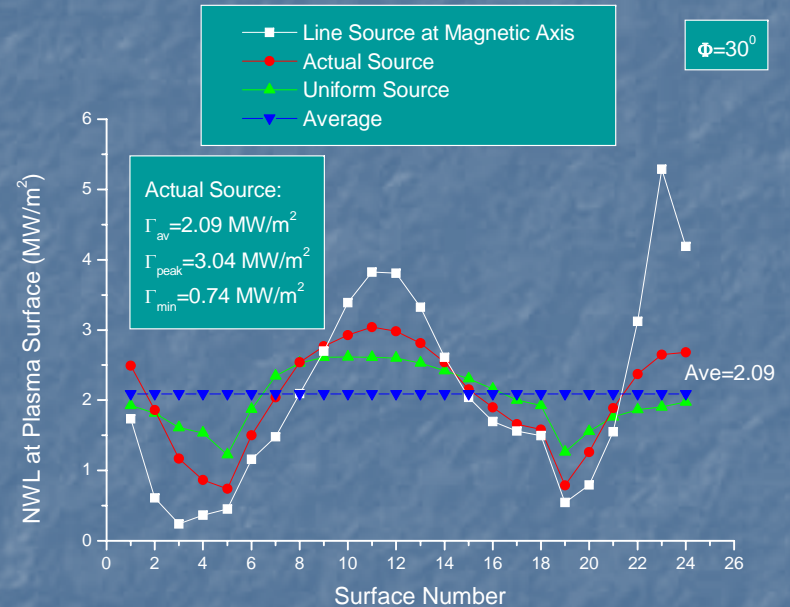
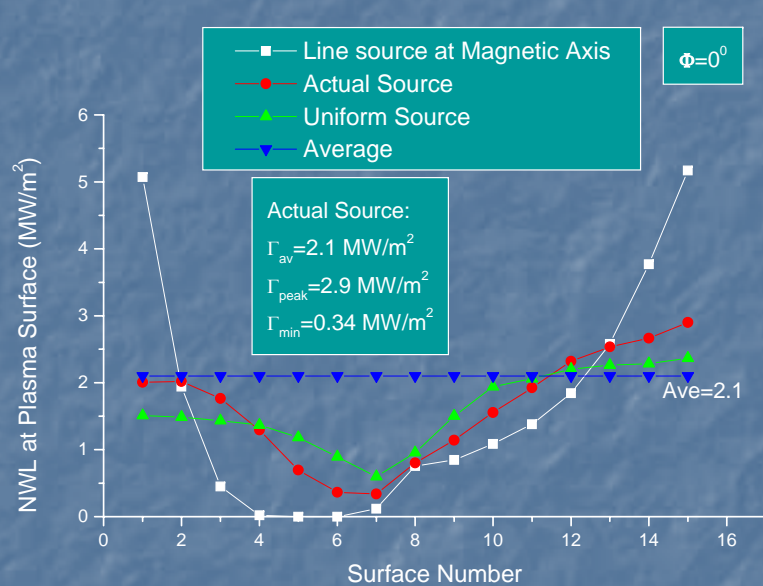


Second step: Cross Section Sweep Object

$\phi=0^\circ$
and
 $\phi=30^\circ$

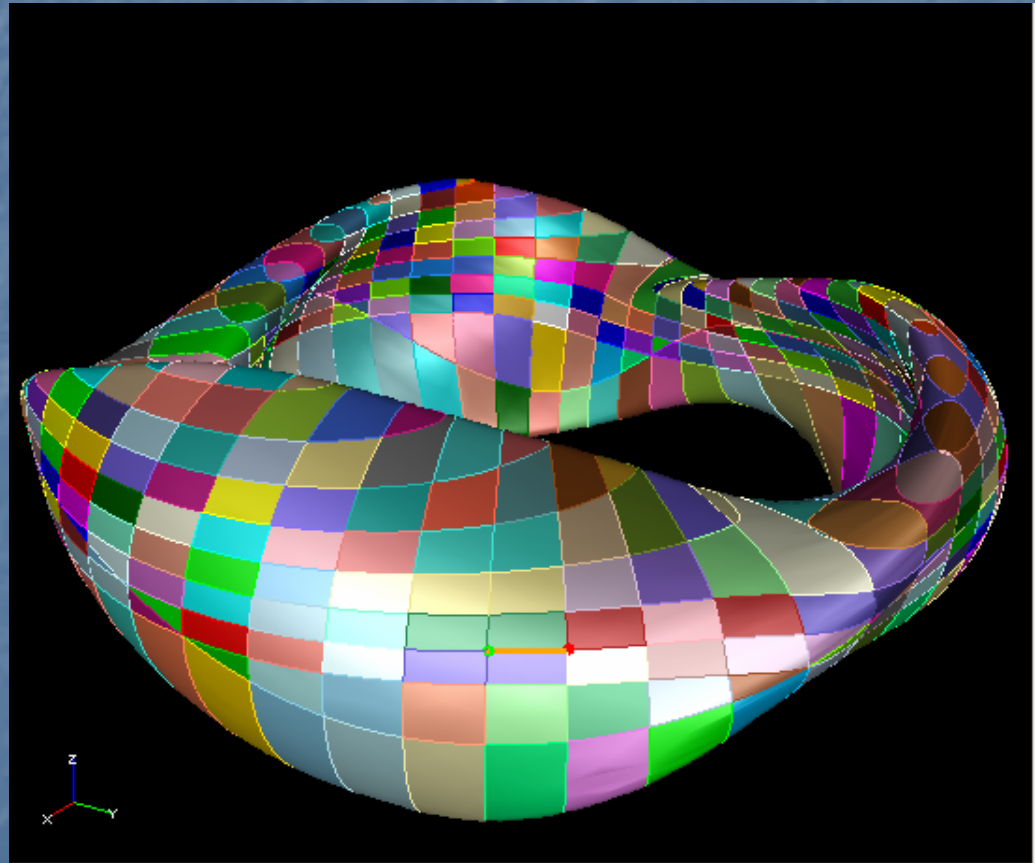


Cross Section Sweep Object (cont)



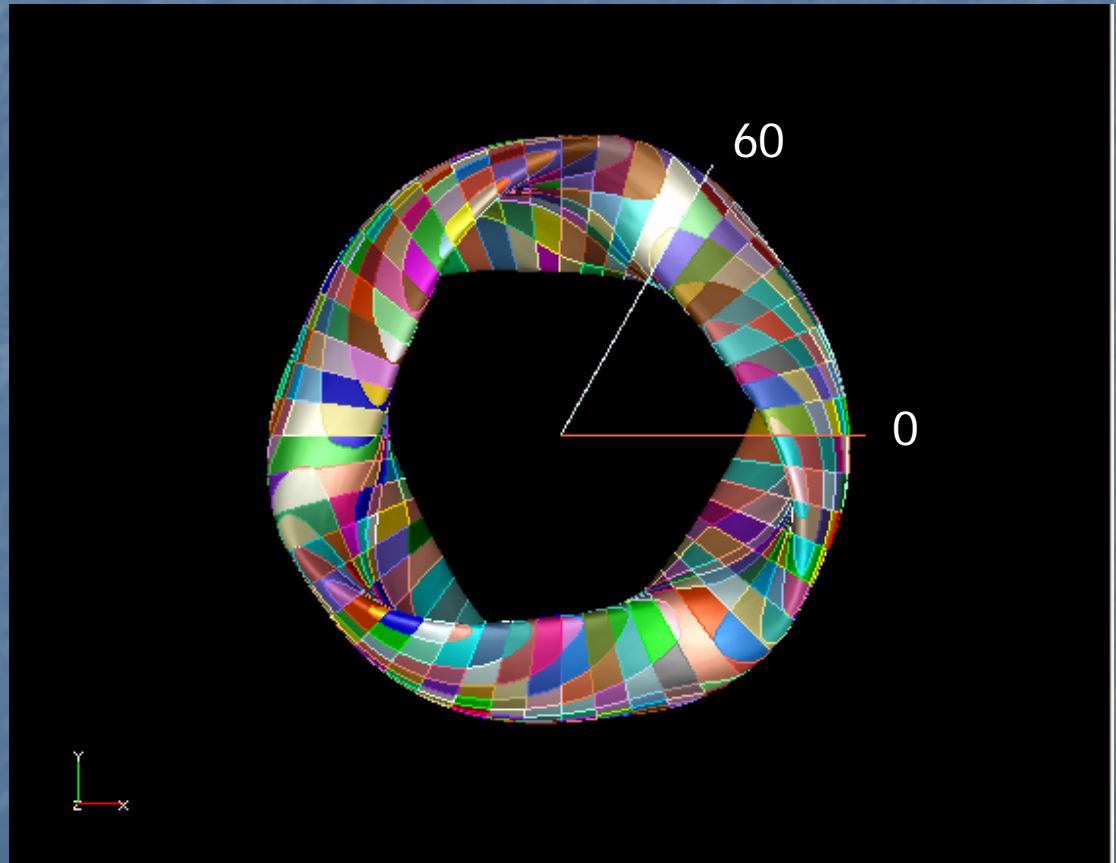
Third step: Computation model of stellerator

- Horizon and toroidal subdivision, each patch as tally surface
 - 7.5 degree toroidal subdivision
 - 0.5 m horizontal subdivision
- Combine the symmetry patch to reduce relative error
- 5 days on a 2.4GHz linux station
- 9% ~ 10% relative error

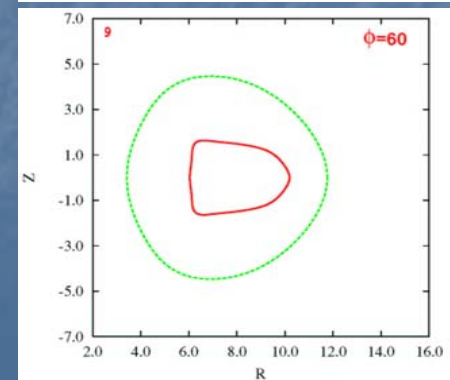
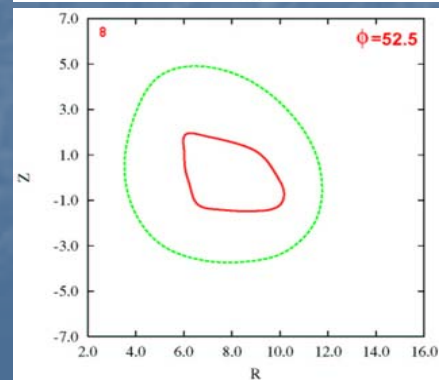
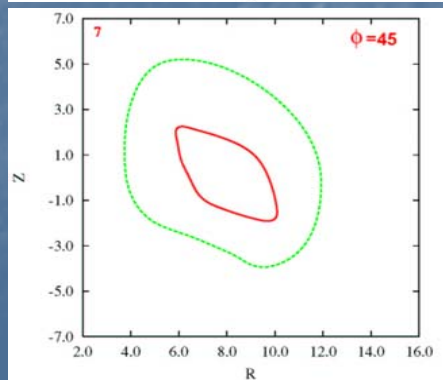
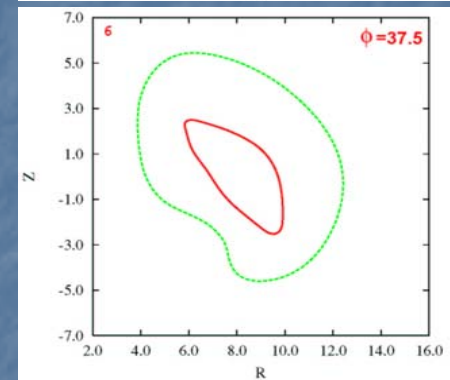
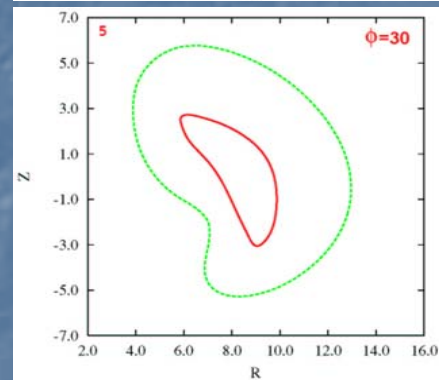
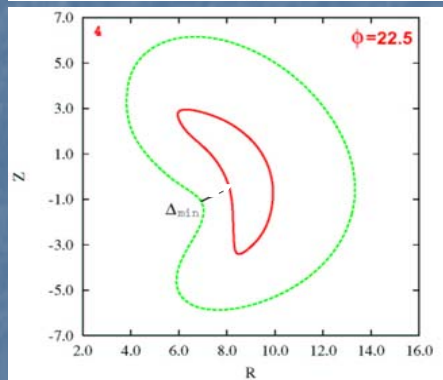
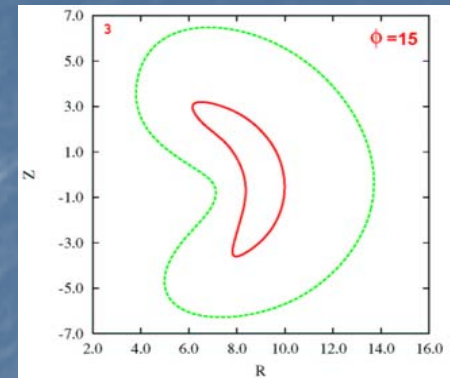
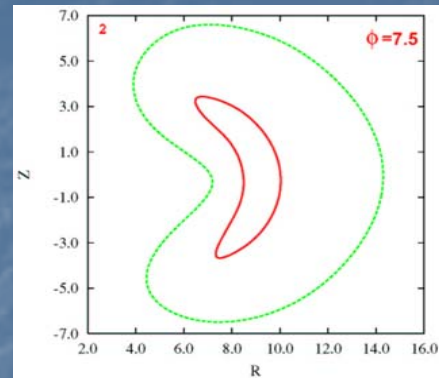
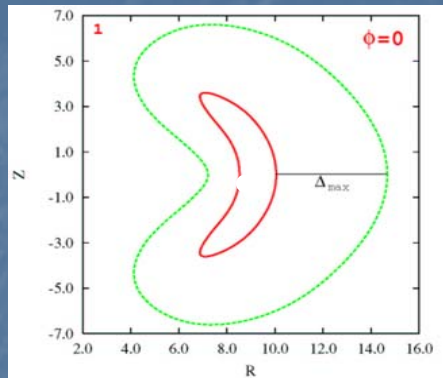


Computation model of stellerator

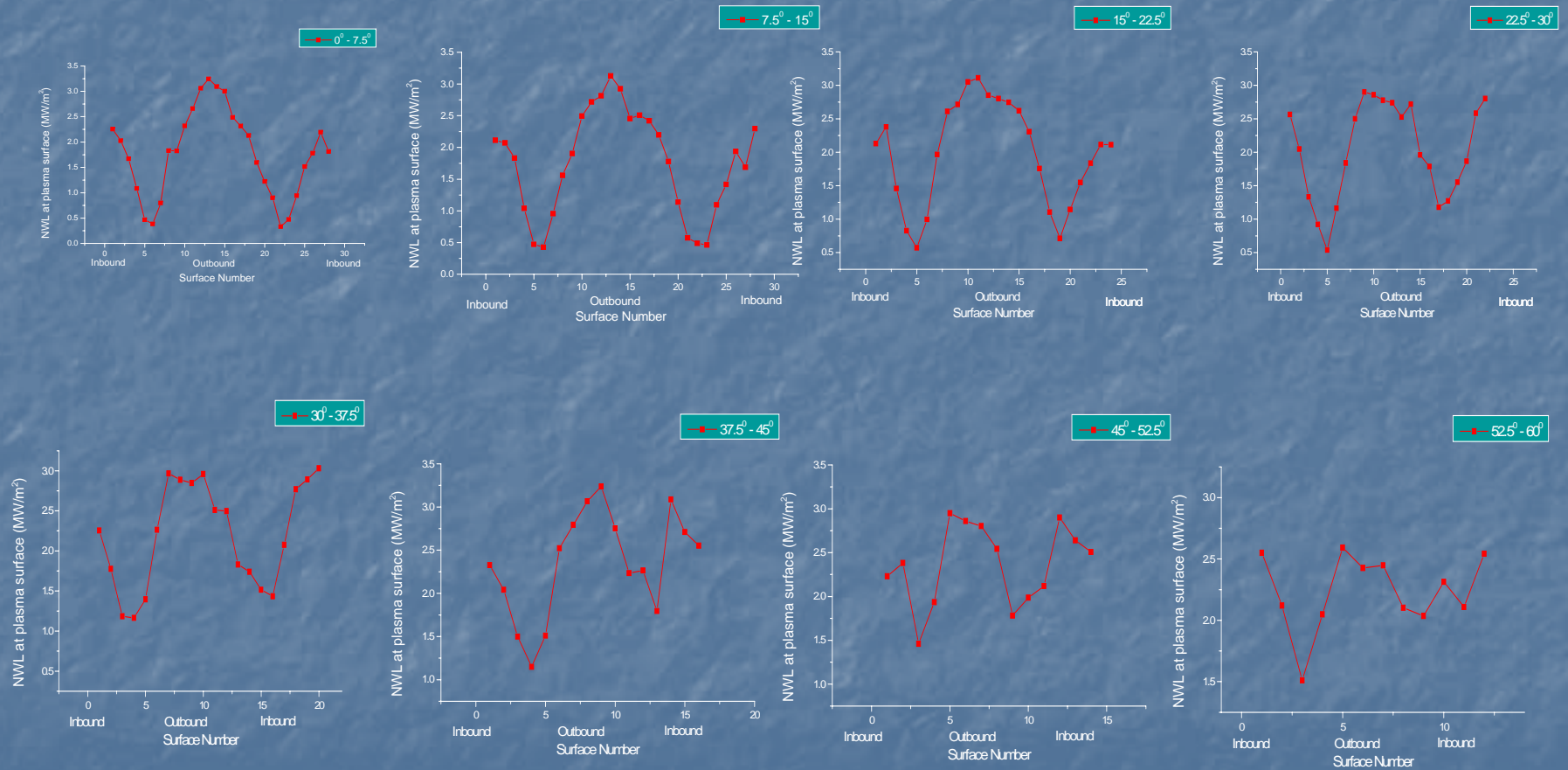
- By the symmetry, select portion from 0 to 60 degree
- 9 cross sections
- 8 neutron wall load profiles



9 Cross Section of Plasma Boundary (red) and WP Center (green)



Computation result

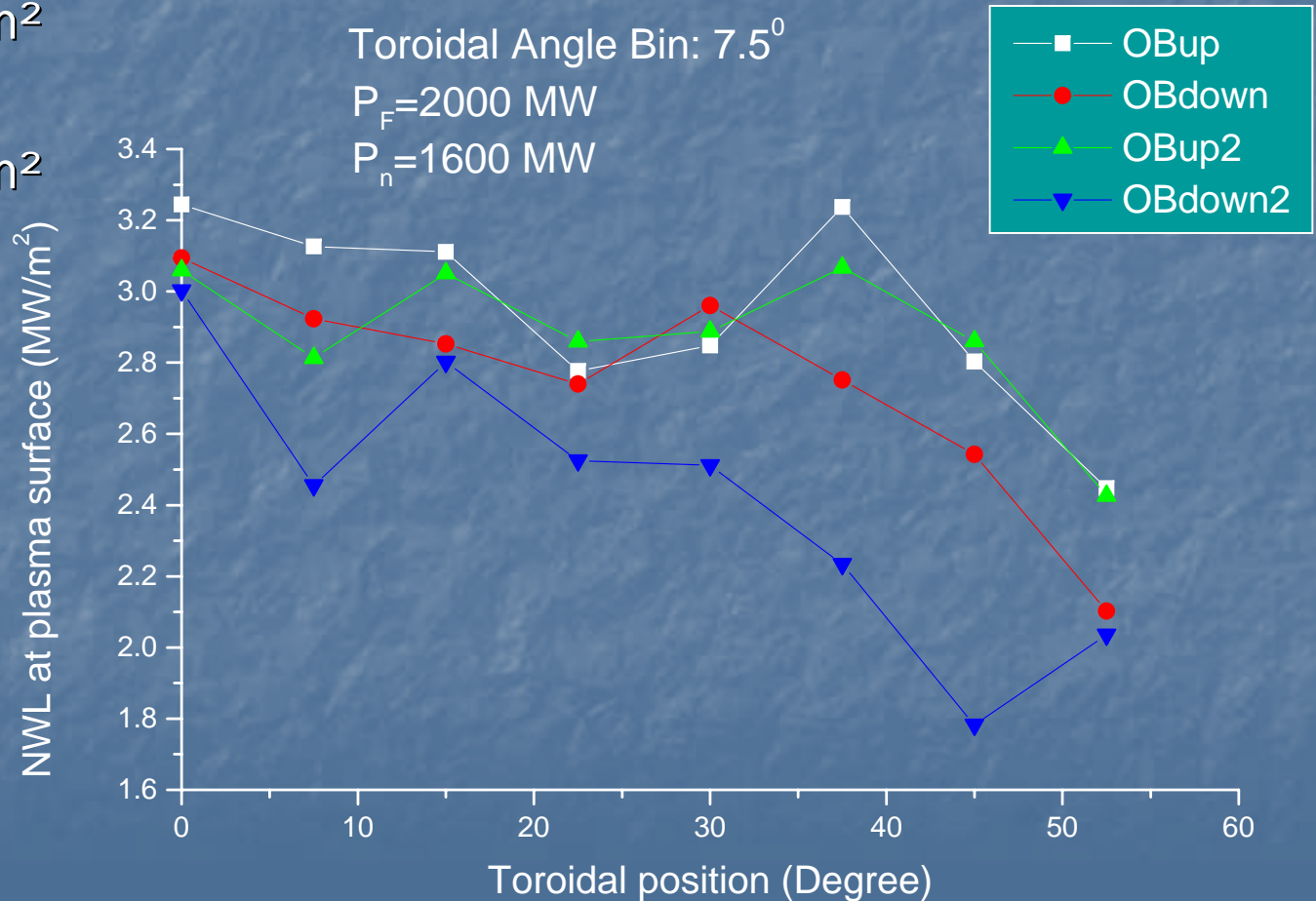


Peak is at Outbound

$\Gamma_{\text{peak}}=3.24\text{MW/m}^2$

$PS_{\text{area}}=800.6\text{m}^2$

$\Gamma_{\text{ave}}=1.985\text{MW/m}^2$



Problem of CAD based MCNP

- Performance of CGM/MCNP
 - CAD based MCNP is about 10 – 30 times slower than standard MCNP
- Reason
 - CAD function is not optimized for a single function
 - Ray-object intersection function is compatible with all type of geometry
 - Ray-object intersection function also test for vertex and edge

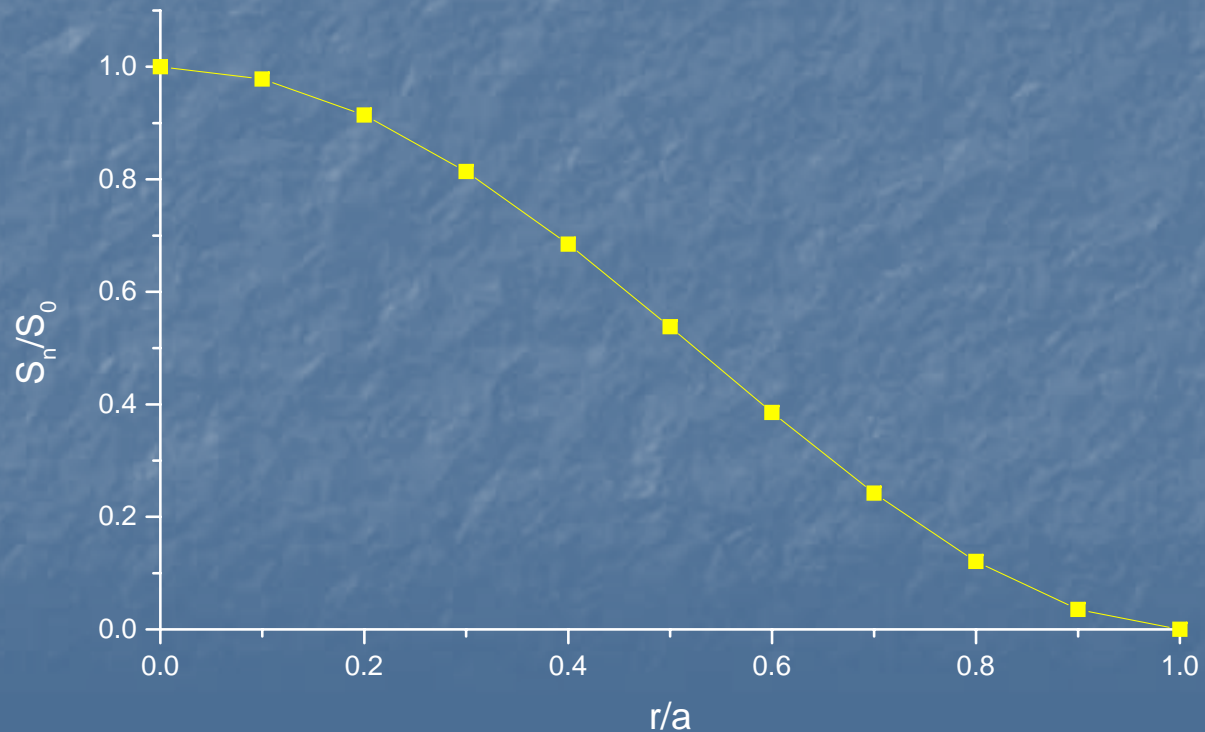
Future Plan

- Speed up calculations
 - Bounding box
 - Spatial subdivision
 - Direction techniques

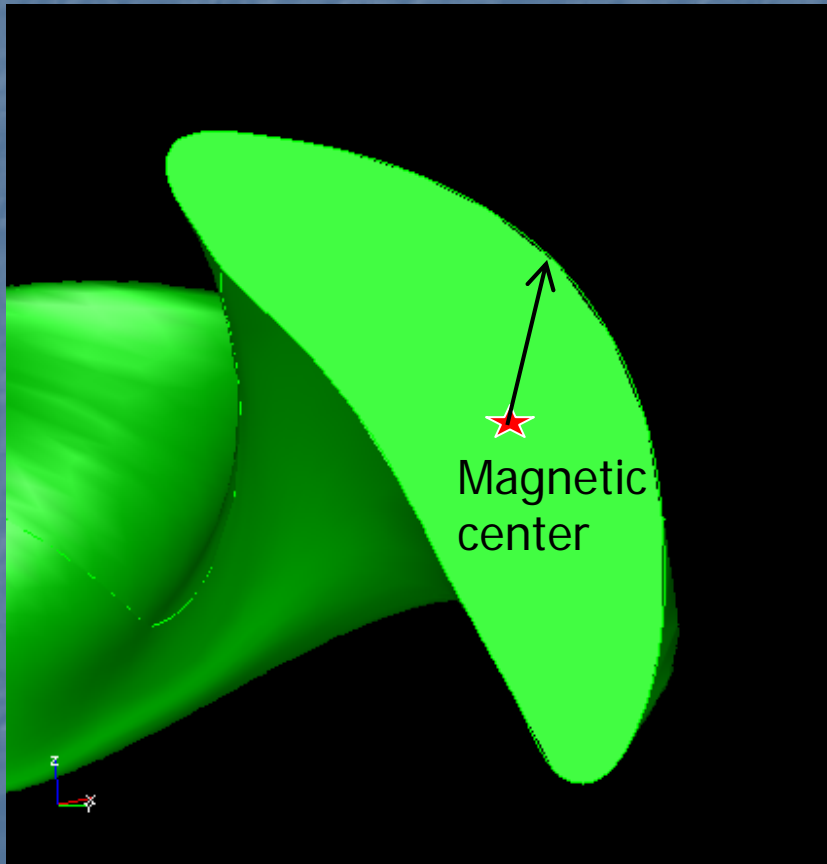
Neutron Source Profile

- the neutron production rate (in $cm^{-3}s^{-1}$)

$$S_n(r/a) = S_0 [1 - 0.2(r/a)^2]^2 [1 - (r/a)^2]^{1.8}$$



Plasma Cross Section



- 'a' is calculated by CAD ray-fire function
 - Start from magnetic center
 - Direction is determined by sampling toroidal and poloidal direction

Neutron Source Profile

- 'r' is from magnetic center
 - Center position is computed by a constant table and two formula.
 - Constant Table

n	rmag	zmag
0	8.5672E+00	0.0000E+00
1	6.0678E-01	-2.9852E-01
2	4.1392E-02	-1.8349E-02
3	-2.2776E-03	1.2718E-03
4	-1.1638E-03	7.3849E-04
5	-9.5859E-04	-9.9194E-06
6	-6.2693E-05	6.6409E-05
 - in the following formula;
$$R = \sum \{ \text{rmag}(n) * \cos(np * n * \text{phi}) \}$$
$$Z = \sum \{ \text{zmag}(n) * \sin(np * n * \text{phi}) \}$$
- 'a' is from magnetic center to plasma surface
 - Use a CAD ray-fire function obtain 'a'.